

Table 1 Chemical composition of the experimental Al-Si-Cu-Mg alloys measured by inductively coupled plasma atomic emission spectroscopy (ICP-AES), wt.%.

| Alloys | Al | Si | Cu | Mg | Ti | Zr | Mn | Cr | Fe | Ni | V | Zn | Sr |
|-------------|-----|------|------|------|------|-------|-------|-------|------|-------|-------|-------|-------|
| Baseline | Rem | 6.79 | 0.51 | 0.35 | 0.11 | 0.002 | 0.008 | 0.001 | 0.09 | 0.004 | 0.017 | 0.008 | 0.015 |
| Zr-modified | Rem | 8.59 | 0.79 | 0.37 | 0.12 | 0.14 | 0.008 | 0.001 | 0.10 | 0.004 | 0.010 | 0.010 | 0.017 |

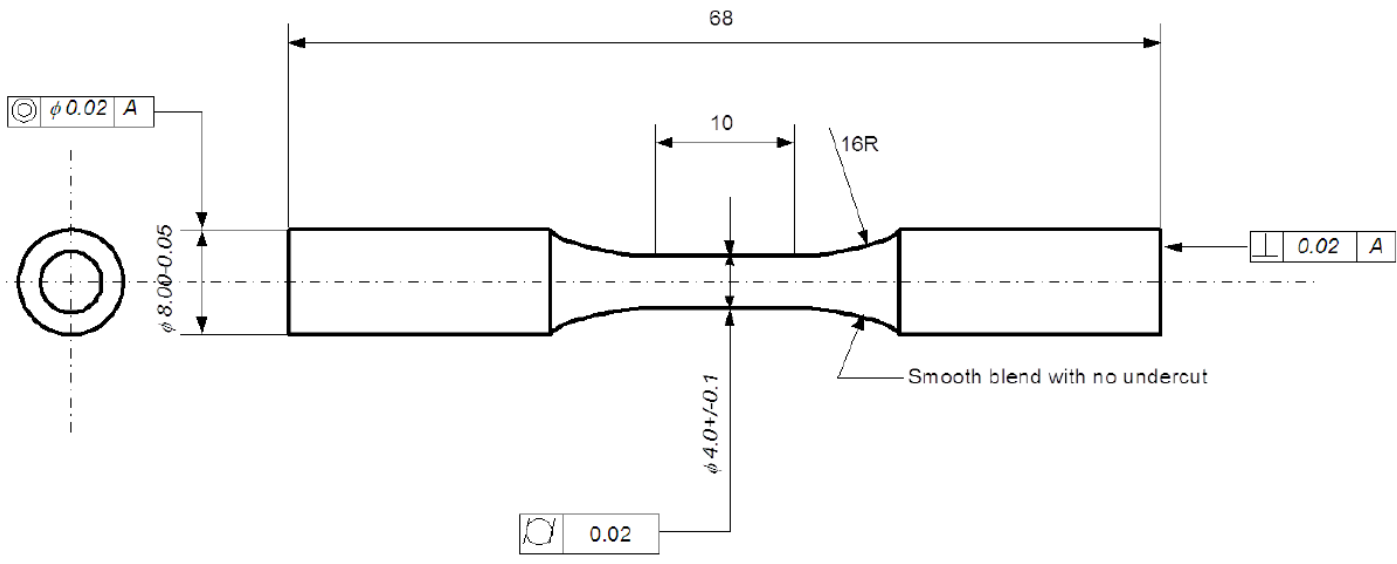


Figure 1 The geometry and dimension of the specimen subjected to the high cycle fatigue test.

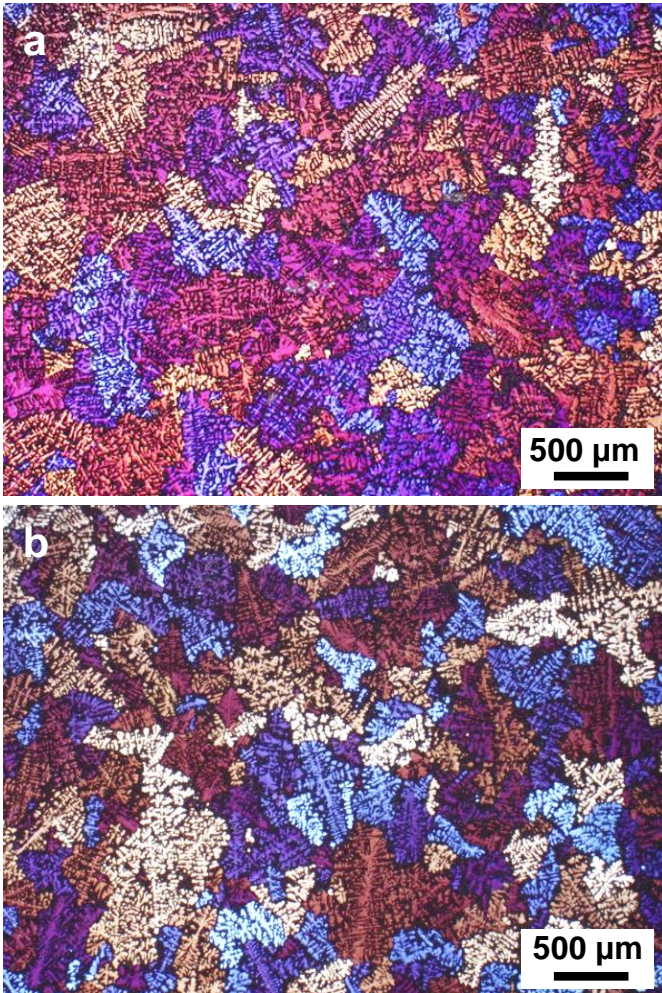


Figure 2 Optical micrographs showing the grain size of (a) baseline, and (b) Zr-modified Al-Si-Cu-Mg alloys after T6 heat treatment.

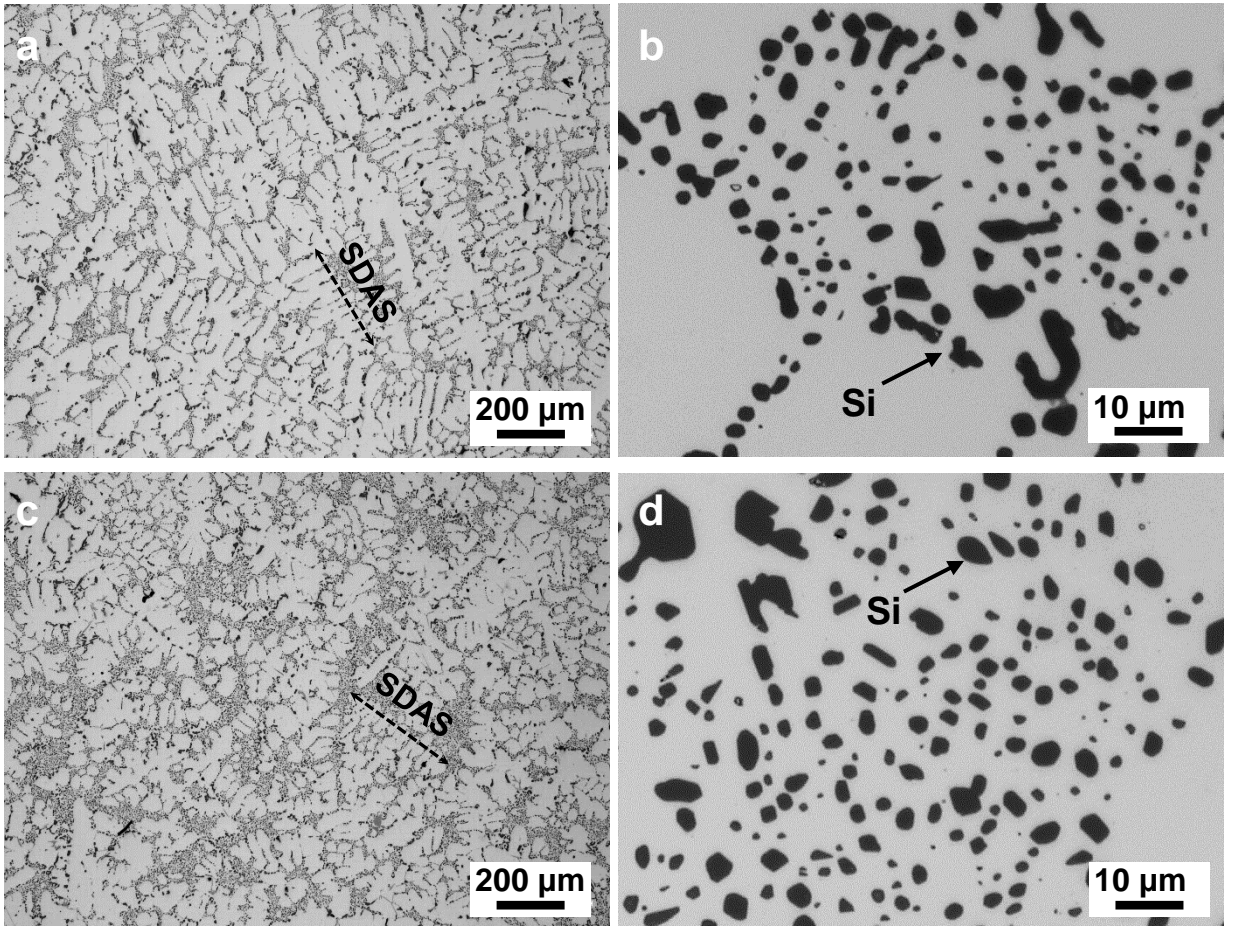


Figure 3 Optical micrographs showing the primary α -Al and eutectic Si phases of (a, b) baseline, and (c, d) Zr-modified Al-Si-Cu-Mg alloys after T6 heat treatment.

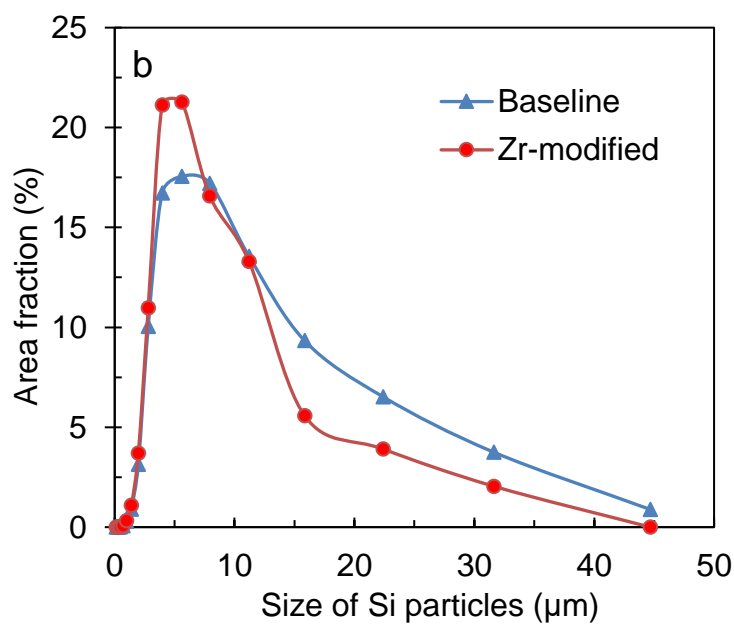
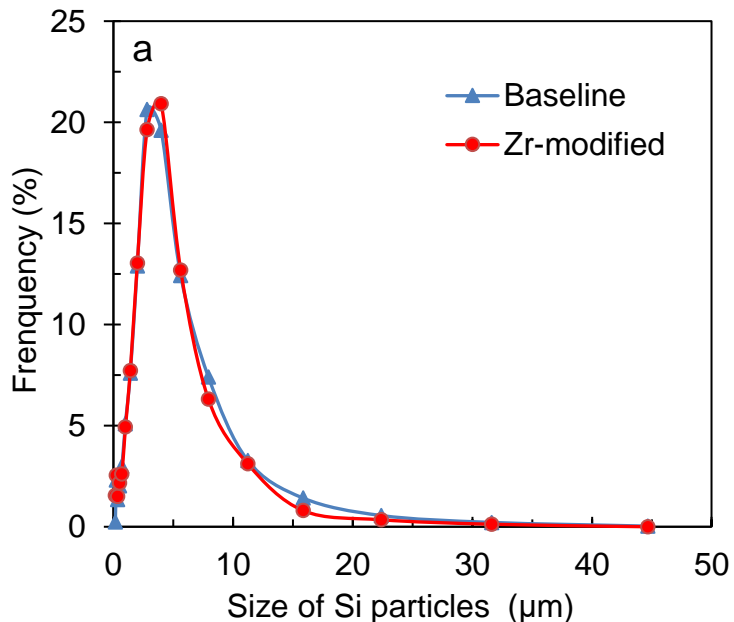


Figure 4 The size distribution of the Si particles of the baseline and Zr-modified Al-Si-Cu-Mg alloys after T6 heat treatment. (a) number fraction, and (b) area fraction. More than 10000 individual Si particles were statistically measured.

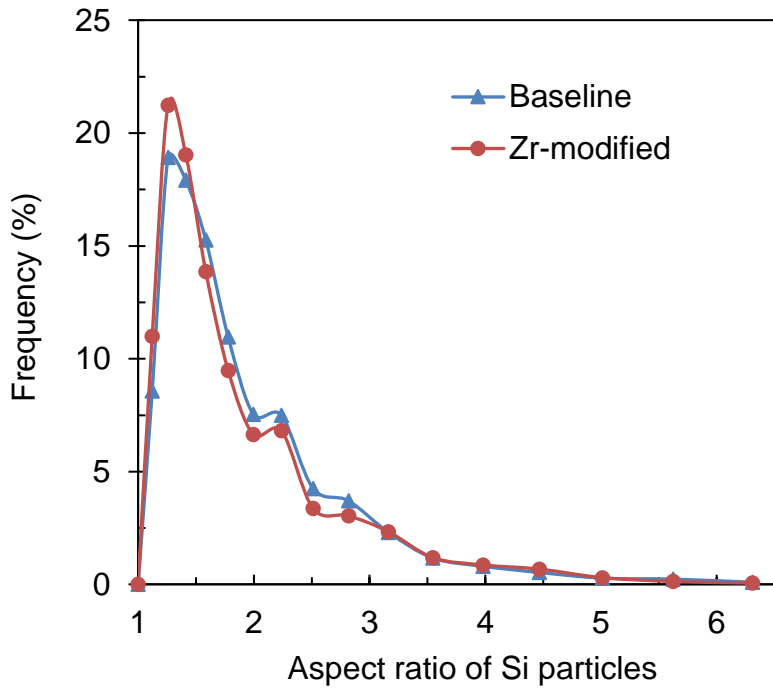


Figure 5 The aspect ratio distribution of the Si particles of the baseline and Zr-modified Al-Si-Cu-Mg alloys after T6 heat treatment. More than 10000 individual Si particles were statistically measured.

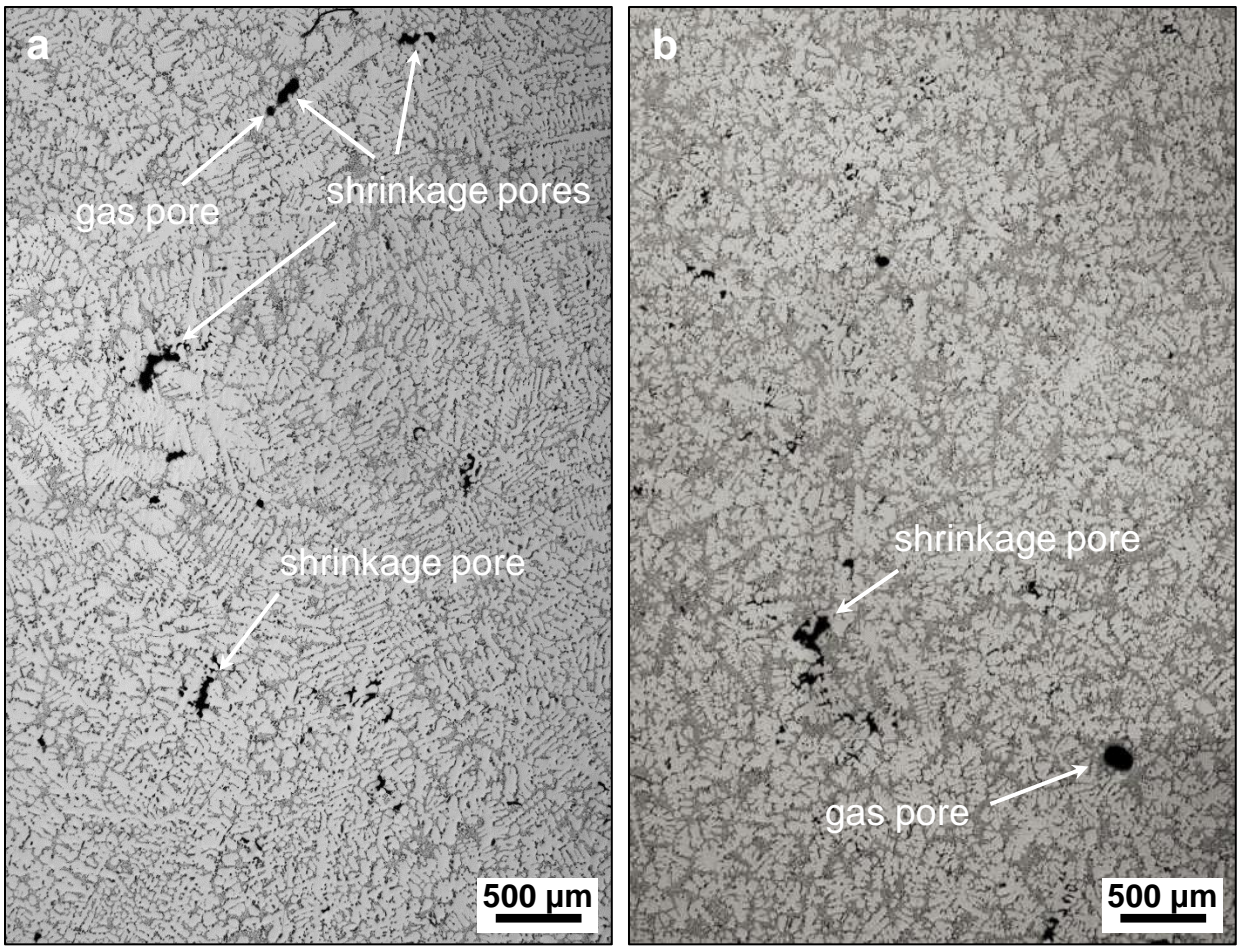


Figure 6 Optical micrographs showing the gas and shrinkage pores of (a) the baseline and (b) Zr-modified Al-Si-Cu-Mg alloys after T6 heat treatment.

Table 2 Comparison of the quantitative metallographic characteristics of α -Al, eutectics, Si particles, and porosities of the experimental Al-Si-Cu-Mg alloys. GS: Grain size, SDAS: Secondary dendrite arm spacing.

| Alloys | α -Al | | Eutectics | Si particles | | Porosities | | |
|-------------|----------------------|------------------------|-------------------|--|-------------------|-------------------|-------------------|--|
| | GS (μm) | SDAS (μm) | Area fraction (%) | Mean Ferret diameter (μm) | Mean aspect ratio | Area fraction (%) | Mean aspect ratio | Mean Ferret diameter (μm) |
| Baseline | 335 \pm 18 | 39 \pm 2 | 27.9 \pm 1.2 | 3.3 \pm 1.9 | 1.65 \pm 0.44 | 0.33 \pm 0.02 | 2.4 \pm 0.1 | 110.2 \pm 11.2 |
| Zr-modified | 253 \pm 41 | 28 \pm 3 | 33.1 \pm 0.9 | 3.1 \pm 1.7 | 1.61 \pm 0.44 | 0.31 \pm 0.03 | 2.0 \pm 0.2 | 106.1 \pm 9.6 |

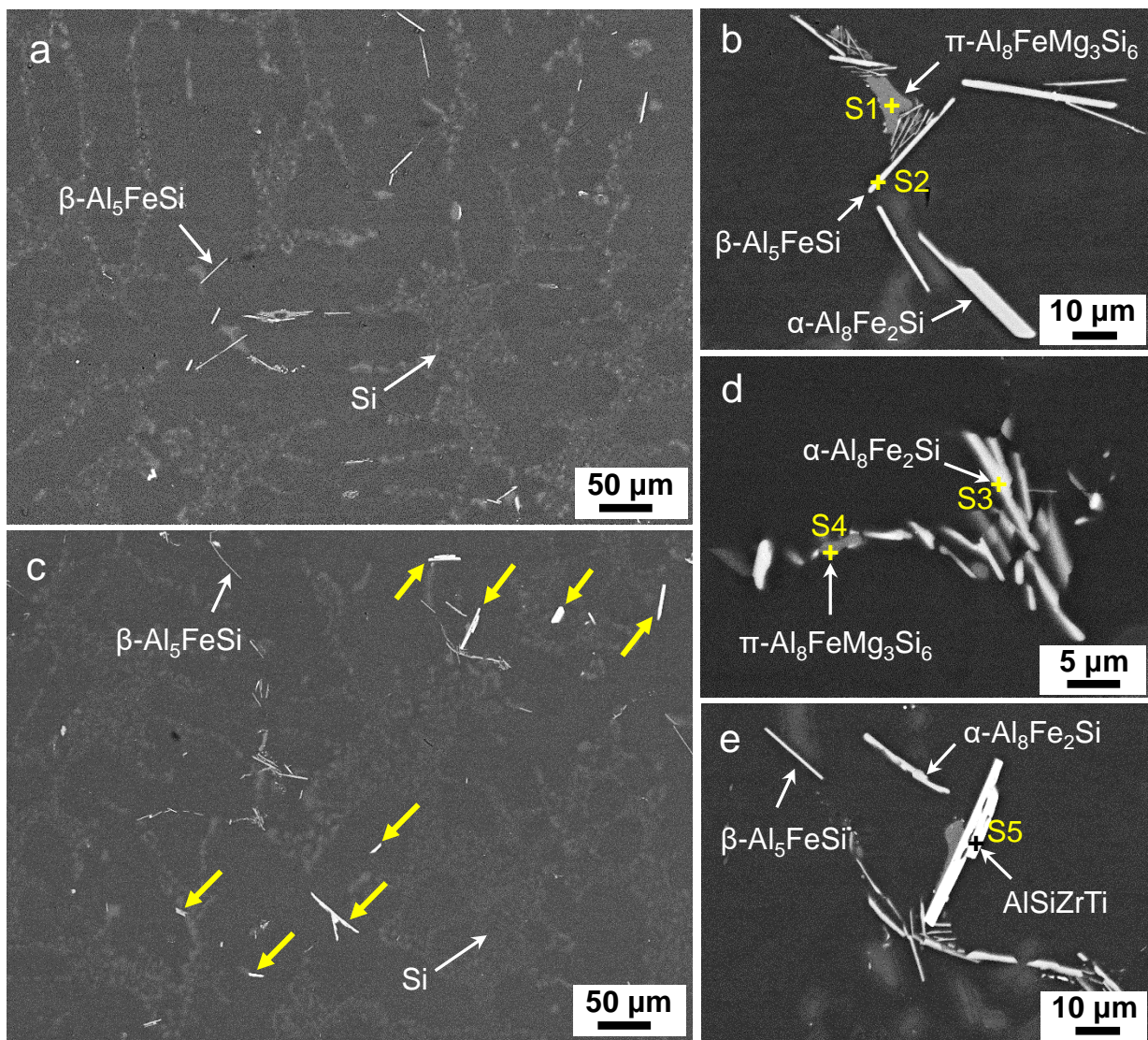


Figure 7 BSE-SEM micrographs showing the Fe-rich and Zr-containing intermetallic phases in the Al-Si-Cu-Mg alloys after T6 heat treatment: (a, b) baseline, and (c, d, e) Zr-modified.

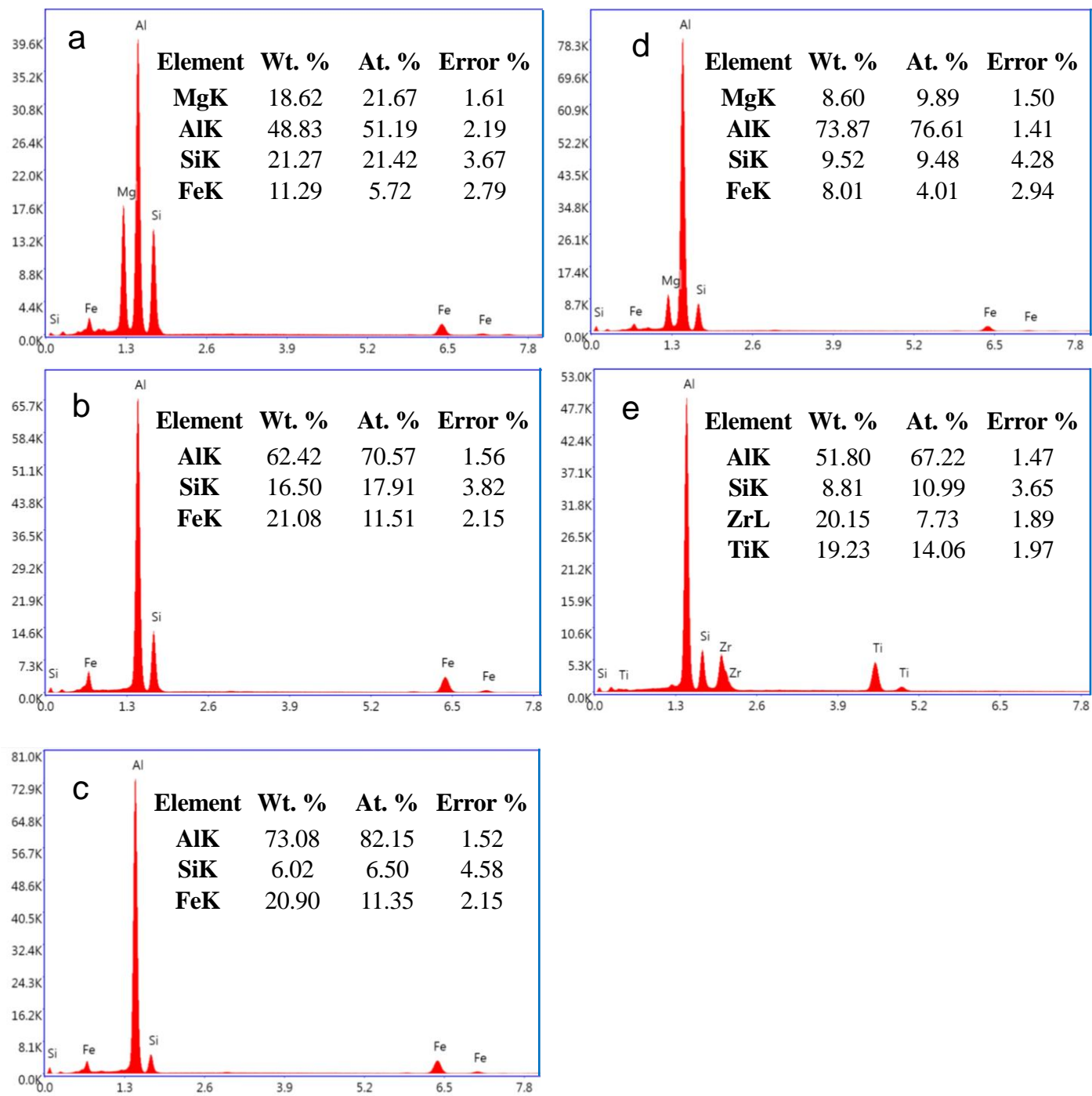


Figure 8 EDS analysis of the Fe-rich and Zr-containing intermetallic phases corresponding to the spectrums in Figure 7: (a) S1, (b) S2, (c) S3, (d) S4, and (e) S5.

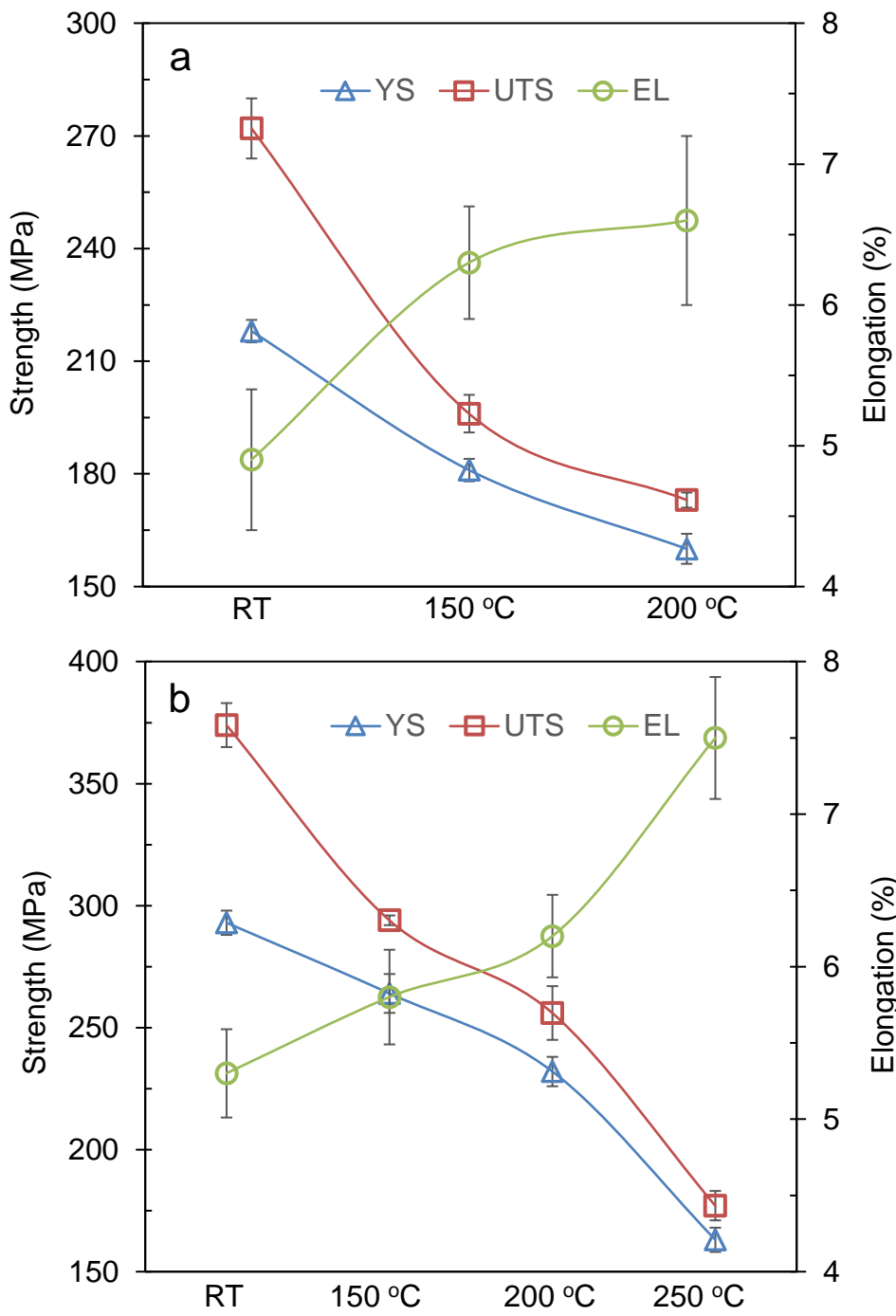


Figure 9 Tensile properties of (a) the baseline and (b) Zr-modified Al-Si-Mg-Cu alloys at different temperatures, RT: room temperature.

Table 3 The tensile properties of the baseline and Zr-modified Al-Si-Cu-Mg alloys tested at room and elevated temperatures.

| Alloys | Test conditions | YS (MPa) | UTS (MPa) | EL (%) |
|---------------|------------------------|-----------------|------------------|---------------|
| Baseline | RT | 218 | 272 | 4.9 |
| | 150 °C | 181 | 196 | 6.3 |
| | 200 °C | 160 | 173 | 6.6 |
| Zr-modified | RT | 293 | 374 | 5.3 |
| | 150 °C | 264 | 294 | 5.8 |
| | 200 °C | 232 | 256 | 6.2 |
| | 250 °C | 163 | 177 | 7.5 |

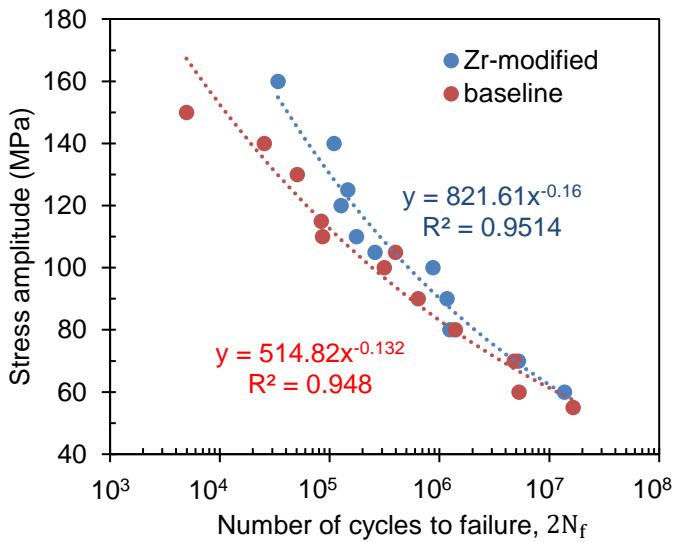
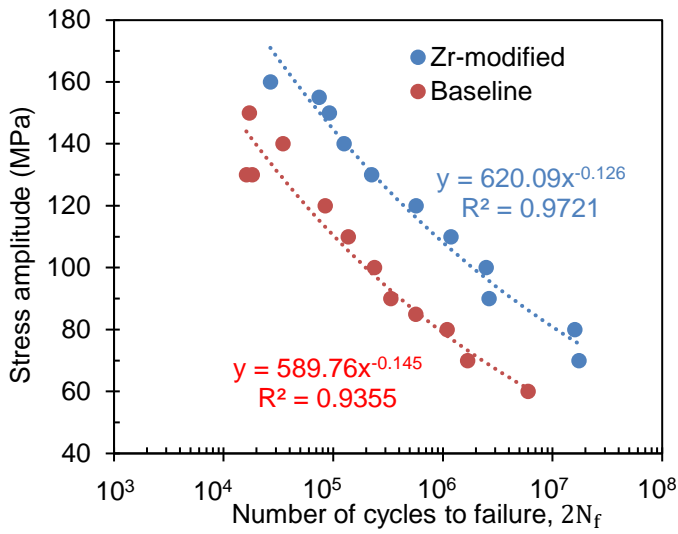
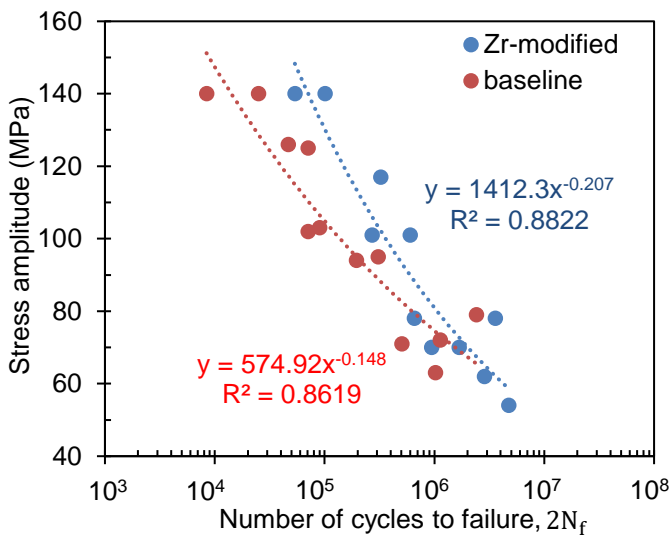


Figure 10 S-N curves of the baseline and Zr-modified Al-Si-Mg-Cu alloys tested at (a) 150 °C, (b) 200 °C, and (c) 250 °C.

Table 4 The fatigue strength coefficient (σ_f') and fatigue strength exponent (b) of the baseline and Zr-modified Al-Si-Cu-Mg alloys tested at 150, 200, and 250 °C, $\sigma_a = \sigma_f' (2N_f)^b$.

| Materials | 150 °C | | | 200 °C | | | 250°C | | |
|-------------|----------------------|--------|-------|----------------------|--------|-------|----------------------|--------|-------|
| | σ_f' (MPa) | b | R^2 | σ_f' (MPa) | b | R^2 | σ_f' (MPa) | b | R^2 |
| Baseline | 574.9 | -0.148 | 0.841 | 589.8 | -0.145 | 0.960 | 514.8 | -0.132 | 0.960 |
| Zr-modified | 1412.3 | -0.207 | 0.861 | 620.1 | -0.126 | 0.973 | 821.6 | -0.160 | 0.959 |

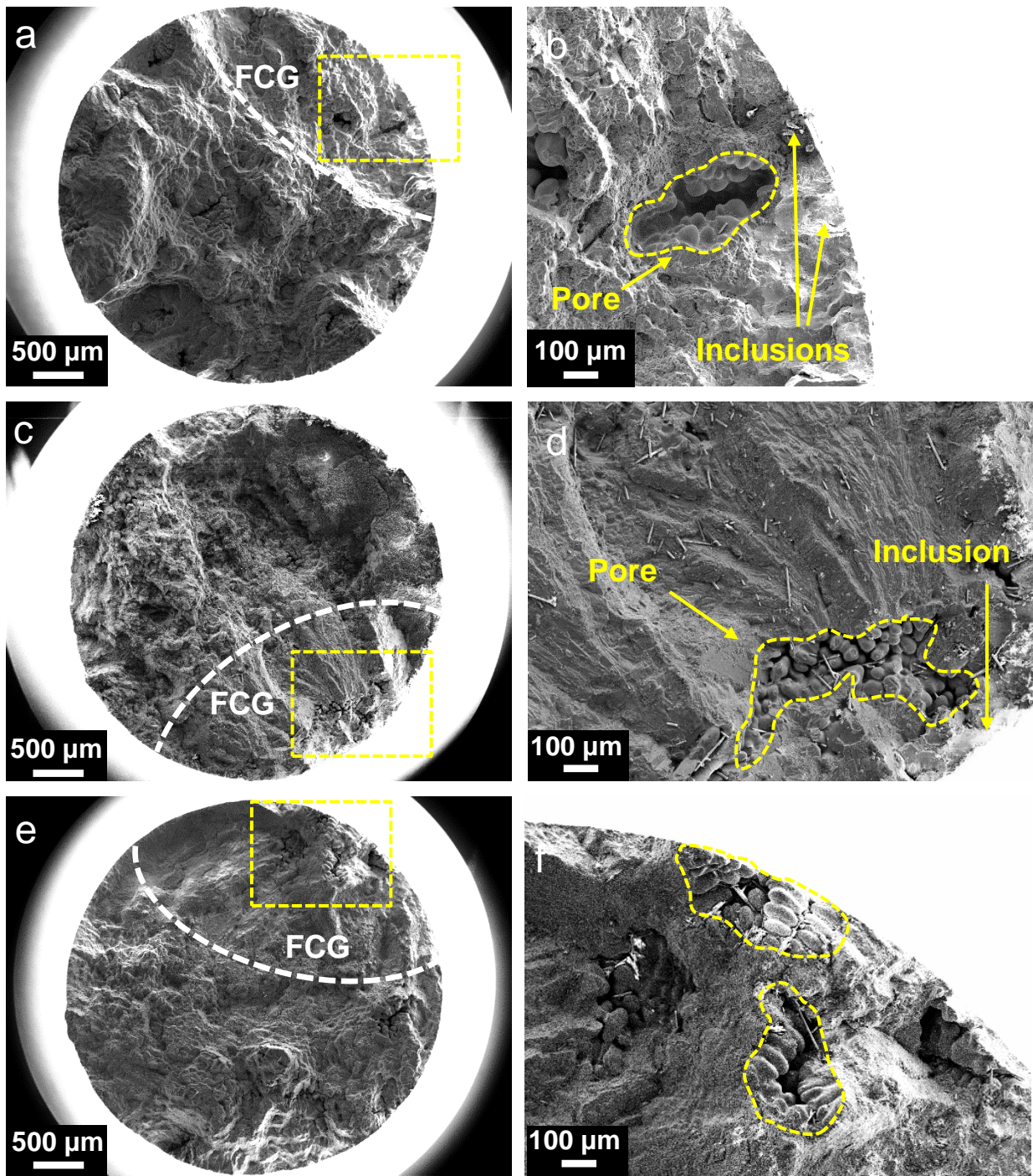


Figure 11 SEM micrographs showing the fatigue fracture surface of the baseline Al-Si-Cu-Mg alloys tested at 200 °C under different stress amplitudes of (a, b) 150 MPa, (c, d) 100 MPa, and (e, f) 70 MPa. FCG: Fatigue crack growth, FCI: Fatigue crack initiation.

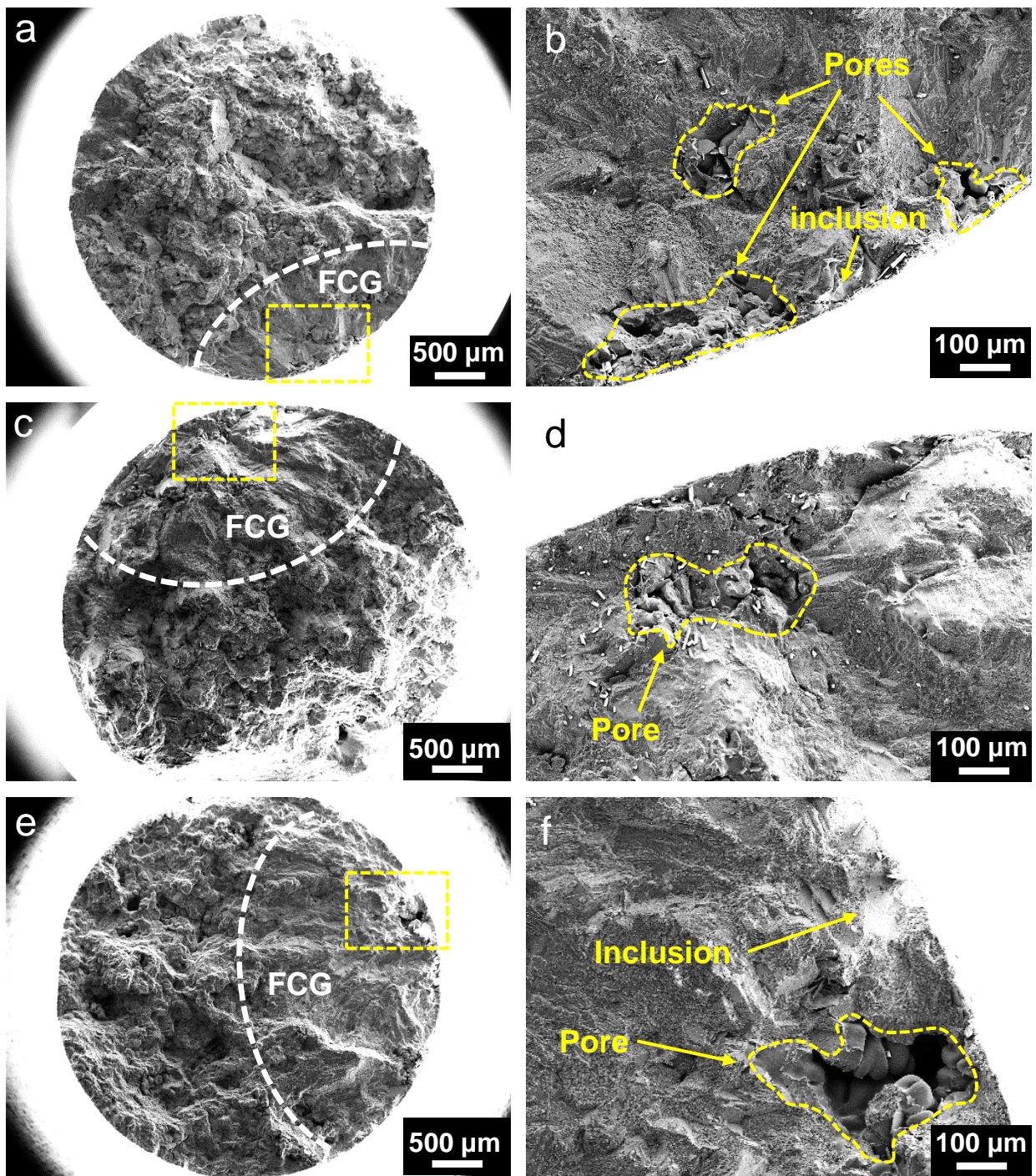


Figure 12 SEM micrographs showing the fatigue fracture surface of the Zr-modified Al-Si-Cu-Mg alloys tested at 200 °C under different stress amplitudes of (a, b) 150 MPa, (c, d) 100 MPa, and (e, f) 70 MPa. FCG: Fatigue crack growth, FCI: Fatigue crack initiation.

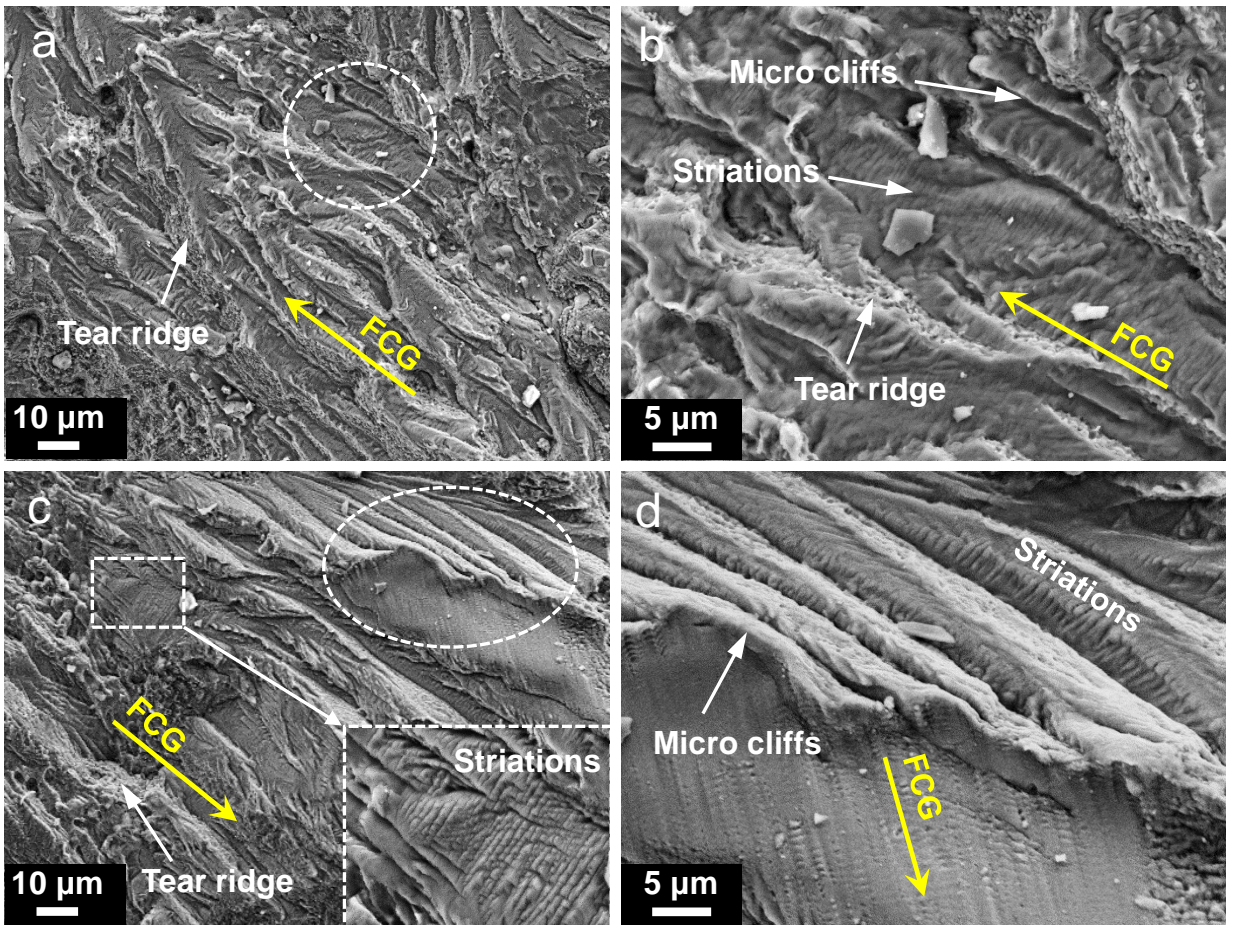


Figure 13 SEM micrographs of fatigue fracture surface, showing the fatigue crack growth of (a, b) the baseline and (c, d) Zr-modified Al-Si-Cu-Mg alloys tested at 200 °C under fatigue stress amplitudes of 100 MPa. FCG: Fatigue crack growth.

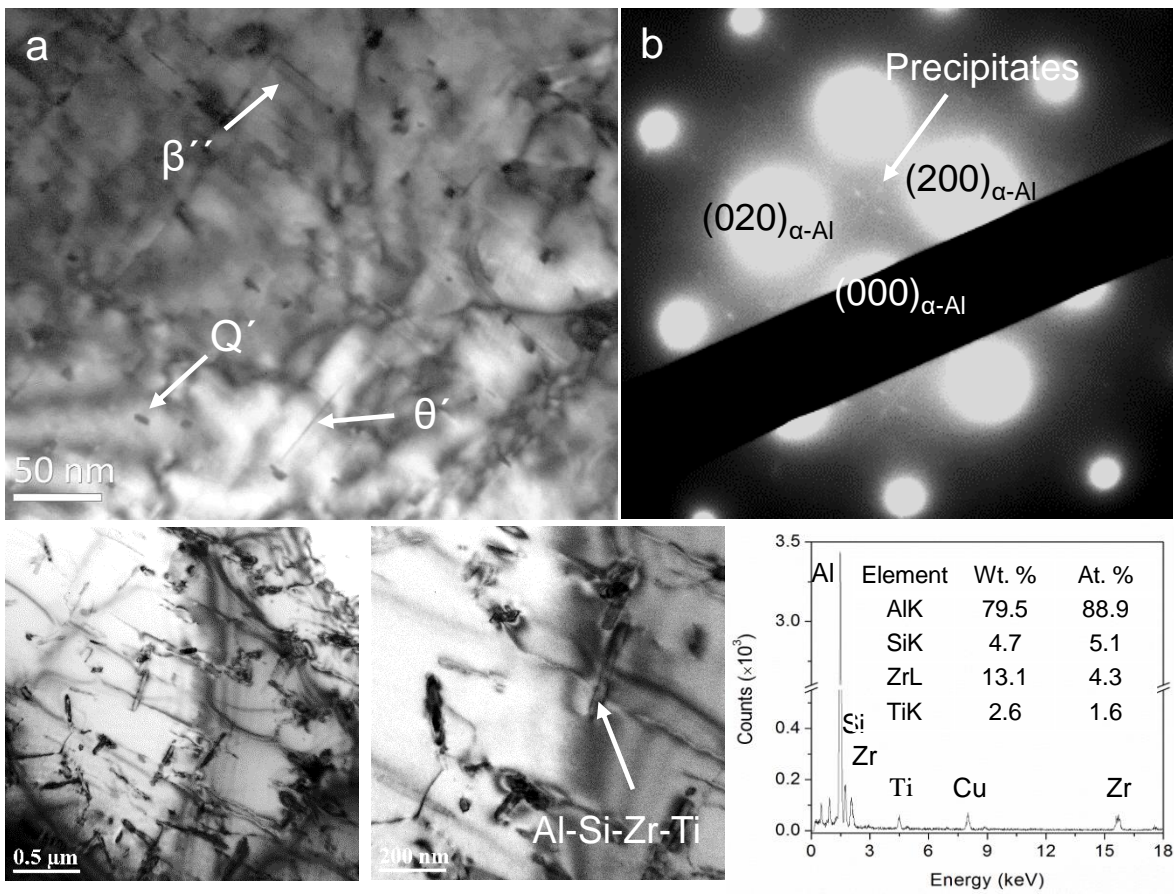


Figure 14 Bright-field TEM micrographs and EDS results, showing (a) the β'' , θ' , and Q' precipitate phases and (b) corresponding SADP in the baseline Al-Si-Cu-Mg alloy; (c, d) the Al-Si-Zr-Ti precipitates in the Zr-modified Al-Si-Cu-Mg alloy, (e) the EDS results corresponding to the spectrum marked in (d).