

# Heterogeneous Nucleation of $\alpha$ -Al on naturally formed $\text{MgAl}_2\text{O}_4$ Particles during Solidification of Al-Mg-Si-Fe-Mn alloys

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## Abstract

The nature of the native  $\text{MgAl}_2\text{O}_4$  particles found in an Al-5Mg-2Si-0.7Mn-1.1Fe alloy was investigated with scanning electron microscopy (SEM) and high-resolution transmission electron microscopy (HRTEM). An orientation relationship (OR) was identified to be:  $8.5^\circ (-1\ 1\ -1)[-1\ 1\ 0]_{\alpha\text{-Al}} // (2\ -2\ 2)[-1\ 1\ 0]_{\text{MgAl}_2\text{O}_4}$ . Different from the OR between the  $\alpha$ -Al and the  $\text{MgAl}_2\text{O}_4$  particles with a “clean” surface [1], a tilt angle ( $8.5^\circ$ ) was observed. The atomic templating layer during the nucleation process of  $\alpha$ -Al on  $\text{MgAl}_2\text{O}_4$  was investigated by considering the interfacial segregation. The contribution of native  $\text{MgAl}_2\text{O}_4$  particles to the grain refinement was investigated.

**Keywords:**  $\text{MgAl}_2\text{O}_4$ , heterogeneous nucleation, tilt angle, interfacial segregation, Al-5Mg-2Si-0.7Mn-1.1Fe alloy

## 1. Introduction

Traditionally, grain refiners are added into liquid melts to refine the average grain size, consequently improving the mechanical properties of the alloys [2-5]. The mechanism of grain refinement with inoculants was understood as supplying of potent particles for heterogeneous nucleation and by alloying to control the surfaces of such refiners or reduce the rate of grain growth [5]. Some grain refiners, such as Al-5Ti-1B master alloy has been successfully developed to refine some Al based alloys [7]. The  $\text{TiB}_2$  particles with “clean” surface are not potent for nucleation of  $\alpha$ -Al due to the larger lattice misfit ( $-4.2\%$ ) with  $\alpha$ -Al compared to others such as  $\text{Al}_3\text{Ti}$  and  $\alpha$ -Al ( $0.09\%$ ). However,  $\text{TiB}_2$  particles in commercial Al-5Ti-1B grain refiner which have an  $\text{Al}_3\text{Ti}$  templating layer [8] is very potent for nucleation of  $\alpha$ -Al due to a very small lattice mismatch at the interface between the  $\text{Al}_3\text{Ti}$  layer and  $\alpha$ -Al. However, the  $\text{TiB}_2$  particles from the grain refiners are not suitable for all of Al alloys. For example, it was reported that, when alloy elements such as Si [9-10], Zr [3, 11] are present in Al alloys, the  $\text{Al}_3\text{Ti}$  layer is dissolved [11]. Therefore, the  $\text{TiB}_2$  particles in Al-5Ti-1B master alloy become not potent, resulting in a coarse grain structure. These results indicate that the nucleation potency of a substrate can change significantly by changing the interface through interfacial segregation or other chemical interactions at the interface. Therefore, investigation on the interaction between melt including impurities and nucleation substrates including both external grain refiners and native inoculant particles in alloy melts are very important to enhance heterogeneous nucleation and achieve the final grain refinement.

40 Oxides particles are unavoidable in Al alloy melts during the casting process, which could act  
41 as substrates for heterogeneous nucleation. Some common oxides in Al-alloys are  $\text{MgAl}_2\text{O}_4$   
42 and  $\alpha\text{-Al}_2\text{O}_3$ . The effect of Mg additions on the oxides in liquid Al alloys have been extensively  
43 investigated in the last decades and show that Mg addition favours the formation of  $\text{MgAl}_2\text{O}_4$   
44 [12-15]. In this study, the major oxide was identified as  $\text{MgAl}_2\text{O}_4$  particles in an Al-5Mg-2Si-  
45 0.7Mn-1.1Fe alloy which contains Mg as high as 5wt.%. The lattice misfits between these in-  
46 situ oxides and the  $\alpha\text{-Al}$  were calculated to be small [16], which means that these particles  
47 should be favourable to nucleate  $\alpha\text{-Al}$ . However, these oxides normally agglomerate in oxide  
48 bi-films [17-18], which reduce their grain refinement efficiency. Recently, some studies have  
49 demonstrated that the in-situ oxide particles can be utilized to enhance the heterogeneous  
50 nucleation when were well-dispersed, and thus achieve grain refinement in Al- and Mg-alloys  
51 especially with the use of the intensive melt shearing technique [16, 19-20]. In particular, it has  
52 been shown that the native  $\text{MgAl}_2\text{O}_4$  particles with {1 1 1} faceted surface nucleated  $\alpha\text{-Al}$  in  
53 Mg-containing Al based alloys [16]. Li. et al investigated the heterogeneous nucleation of  $\alpha\text{-Al}$   
54 on  $\text{MgAl}_2\text{O}_4$  particles in the pure Al. The surface of the naturally formed oxide particles can  
55 be modified due to interfacial segregation in the melt. The atomic templating on the substrate  
56 surface will therefore change during the modification process, and thus affects the lattice  
57 mismatching/ nucleation potency for nucleation [21].

58 In this work, we aimed to investigate the efficiency of native  $\text{MgAl}_2\text{O}_4$  particles for  
59 heterogeneous nucleation of  $\alpha\text{-Al}$  in Al-alloys containing multiple alloying additions. The  
60 oxide films were reduced/eliminated via the intensive melt shearing technique, to investigate  
61 the nature and the efficiency of native  $\text{MgAl}_2\text{O}_4$  for heterogeneous nucleation of  $\alpha\text{-Al}$ . The  
62 effects of interfacial segregation (impurities or the other alloying elements) on the terminating  
63 planes of native  $\text{MgAl}_2\text{O}_4$  particles on the nucleation efficiency were studied by investigating  
64 the orientation relationship changes between the  $\alpha\text{-Al}$  and  $\text{MgAl}_2\text{O}_4$ .

65

## 66 2. Experimental

67 Al-5Mg-2Si-0.7Mn-1.1Fe alloy investigated in this work has a composition of  $5.7\% \pm 0.5\%$  Mg,  
68  $2.1\% \pm 0.2\%$  Si,  $0.65\% \pm 0.04\%$  Mn and  $1.12\% \pm 0.05\%$  Fe (all compositions are in wt.%). The  
69 melting temperature of this alloy is  $668.01^\circ\text{C}$  calculated using the Pandat software using  
70 PanAl2018 database. The starting materials were commercially pure Al ( $>99.86\text{wt.}\%$ ),  
71 commercially pure Mg ( $>99.95\text{wt.}\%$ ), and Al-50Si, Al-20Mn and Al-38Fe master alloys. The  
72 Al-2Si-0.7Mn-1.1Fe alloy melt was prepared at  $750^\circ\text{C}$  in an electric resistance furnace  
73 followed with stirring and sufficiently long holding time to ensure melt homogeneity. The melt  
74 was isothermally held for 30 minutes after Mg addition. To disperse the native inoculant  
75 particles, the intensive melt shearing [22] was used on the alloy melt with shearing unit  
76 operated at 4000rpm for 5 minutes. The melt was cast into a TP 1 mould [23] at  $720^\circ\text{C}$  before  
77 and after intensive melt shearing. In order to facilitate direct examination of oxides particles, a  
78 pressurised melt filtration technique was used after intensive melt shearing to collect the oxide  
79 particles [24].

80

81 The TP-1 sample was sectioned at the cross section at 38mm height from the bottom of the  
82 casting which has a cooling rate of 3.5K/s. The filtration materials immediately above the filter  
83 were sectioned, where the oxide particles were concentrated. Scanning electron microscope  
84 (SEM) observation was carried out with a Zeiss Supera 35 SEM, at accelerating voltages  
85 between 5-20kV. The filtration sample was made into 3mm diameter discs for transmission  
86 electron microscopy (TEM) examinations. The discs were then manually ground to a thickness  
87 of less than 60 $\mu$ m, followed by ion-beam-thinning using a Gatan precision ion polishing system  
88 (PIPS) at energy between 2.0-5.0kV and incident angles of 3-6°. TEM examination was  
89 performed on a JEOL 2100F transmission electron microscope at an accelerating voltage of  
90 200kV equipped with EDX spectroscopy facility operated.

91

### 92 3. Results

93

94 Different types of inoculant particles such as oxides ( $\text{MgAl}_2\text{O}_4$ ), nitride ( $\text{AlN}$ ) and carbide can  
95 be collected from the Al alloys melt, which are reported elsewhere [25-27]. The major type of  
96 inoculant particles in Al-5Mg-2Si-0.7Mn-1.1Fe alloy was identified as  $\text{MgAl}_2\text{O}_4$  (spinel) using  
97 SEM-EDX, TEM-EDX and TEM analyses. Figs.1a-b show the 2- and 3-dimensional  
98 morphology of the native  $\text{MgAl}_2\text{O}_4$  particles collected. The size of these  $\text{MgAl}_2\text{O}_4$  particles  
99 ranges from 0.5 to 1 $\mu$ m. The agglomeration of these  $\text{MgAl}_2\text{O}_4$  particles was rarely observed.

100 The TEM-EDX results from more than 20  $\text{MgAl}_2\text{O}_4$  particles indicated that they have a  
101 composition of O 39.8 $\pm$ 0.5at.%, Mg 20.2 $\pm$ 0.2at.% and Al 40.0 $\pm$ 0.6at.%. The TEM examination  
102 results show that these  $\text{MgAl}_2\text{O}_4$  particles have the face-centred cubic (fcc) crystal structure  
103 with  $a=8.08\pm 0.005\text{\AA}$ , and are {1 1 1} faceted. One such example is shown in Fig.1c. It shows  
104 that the  $\text{MgAl}_2\text{O}_4$  particle is {1 1 1} faceted when viewed along its  $\langle 1\ 1\ 0 \rangle$  zone direction, and  
105 the angles between two adjacent termination planes are measured to be  $109.5 \pm 0.4^\circ$  or  $70.5 \pm$   
106  $0.5^\circ$ .

107 Most of the  $\text{MgAl}_2\text{O}_4$  particles are distributed in the oxides films and have no specific in-plane  
108 orientation relationship with  $\alpha$ -Al. However, those naturally formed  $\text{MgAl}_2\text{O}_4$  particles  
109 observed to be embedded in  $\alpha$ -Al grains, have specific OR with  $\alpha$ -Al, Fig.2. The HRTEM  
110 observation on the  $\alpha$ -Al/ $\text{MgAl}_2\text{O}_4$  interface is shown in Fig.2a. The indexed fast fourier  
111 transform (FFT) patterns from  $\alpha$ -Al and  $\text{MgAl}_2\text{O}_4$  were shown in Fig.2b and c, respectively.  
112 The incident electron beam is parallel to  $\langle 1\ 1\ 0 \rangle$  of  $\alpha$ -Al and  $\langle 1\ 1\ 0 \rangle$  of  $\text{MgAl}_2\text{O}_4$ . This reveals  
113 an orientation relationship (OR) as:  $8.5^\circ(1\ -1\ 1)_{\alpha\text{-Al}} // (2\ -2\ 2)_{\text{MgAl}_2\text{O}_4}$  and  $[-1\ 1\ 0]_{\alpha\text{-Al}} // [-1\ 1\ 0]_{\text{MgAl}_2\text{O}_4}$ .  
114  $(1\ -1\ 1)_{\alpha\text{-Al}}$  and  $(2\ -2\ 2)_{\text{MgAl}_2\text{O}_4}$ . It has an angle of  $8.5^\circ$  between the two planes. This  
115 observation of the OR provides evidence that the in-situ  $\text{MgAl}_2\text{O}_4$  particles do nucleate  $\alpha$ -Al  
116 in Al-5Mg-2Si-0.7Mn-1.1Fe alloy. However, the orientation relationship between  $\{1\ 1\ 1\}_{\alpha\text{-Al}}$   
117 and  $\{1\ 1\ 1\}_{\text{MgAl}_2\text{O}_4}$  has a  $8.5^\circ$  deviation from the reported OR [1] observed on the “clean”  
118  $\text{MgAl}_2\text{O}_4$  surface.

119 In-situ oxide particles in Al alloys always form and contained in the double oxide films  
120 therefore difficult to achieve the effective grain refinement [28-29]. With intensive melt  
121 shearing, these oxide films can be dispersed uniformly allowing them to be more effective  
122 inoculant particles to grain refine the alloys [16, 19-20]. In this study,  $\text{MgAl}_2\text{O}_4$  particles

123 formed as the major native oxides and was confirmed to be the potent nucleation substrates for  
 124  $\alpha$ -Al (Fig.2). Therefore, the nucleation efficiency of the in-situ  $\text{MgAl}_2\text{O}_4$  particles needs to be  
 125 investigated. The microstructure of Al-5Mg-2Si-0.7Mn-1.1Fe alloy applied without and with  
 126 intensive melt shearing is shown in Fig. 3. Quantitative measurement of the grain size is given  
 127 in Table 2. It shows that the average  $\alpha$ -Al grain size was reduced from  $423\pm 47\mu\text{m}$  in the un-  
 128 sheared sample to  $151\pm 22\mu\text{m}$  in the sheared. The  $\alpha$ -Al grains were refined by the dispersing  
 129 naturally formed inoculant particles. Our previous research reported that although the  
 130 equilibrium primary phase of Al-5Mg-2Si-0.7Mn-1.1Fe alloy was calculated to be  $\alpha$ -  
 131  $\text{Al}_{15}(\text{Fe},\text{Mn})_3\text{Si}_2$  ( $\alpha$ -AlFeSi), the primary  $\alpha$ -AlFeSi phase was suppressed when cast at  $720^\circ\text{C}$   
 132 with a cooling rate of  $3.5\text{K/s}$  [30]. Therefore, the effect of the formation of  $\alpha$ -AlFeSi phase on  
 133 the grain refinement of  $\alpha$ -Al can be excluded.

134

#### 135 4. Discussion

136 In this study, the native  $\text{MgAl}_2\text{O}_4$  particles were generated in Al-alloys containing multiple  
 137 additives including Si, Fe and Mn. Those alloying elements were found segregate on  $\text{TiB}_2$   
 138 particles [21]. Therefore, it is possible for these elements to segregate on the  $\text{MgAl}_2\text{O}_4$  particles  
 139 as well. The angle ( $8.5^\circ$ ) between the  $\{1\ 1\ 1\}_{\alpha\text{-Al}}$  and  $\{1\ 1\ 1\}_{\text{MgAl}_2\text{O}_4}$  suggests that the  $\{1\ 1\ 1\}$   
 140 planes of  $\text{MgAl}_2\text{O}_4$  in this alloy may be modified. In this case, the structure of  $\text{MgAl}_2\text{O}_4$   
 141 particles at the nucleation interface is determined by the newly templated atomic layer(s)  
 142 caused by interfacial segregation or chemical interaction rather than the  $\{1\ 1\ 1\}$  planes of  
 143  $\text{MgAl}_2\text{O}_4$ . From another point of view, the  $\alpha$ -Al at the interface with the  $\text{MgAl}_2\text{O}_4$  are not  $\{1\ 1\ 1\}$   
 144 planes but the  $\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}_{\alpha\text{-Al}}$  after accounting for the tilt angle ( $\theta$ ). (where  $x$  is an integer value  
 145 greater than 1). Due to the limited information on the modified  $\{1\ 1\ 1\}$  planes of  $\text{MgAl}_2\text{O}_4$ , we  
 146 focus on the nucleating planes of  $\alpha$ -Al. Consequently, the OR between  $\alpha$ -Al and the native  
 147  $\text{MgAl}_2\text{O}_4$  particles could be considered as  $\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}_{\alpha\text{-Al}}//\{1\ 1\ 1\}_{\text{MgAl}_2\text{O}_4}$ .

148 Based on this discussion, we assumed different  $\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}$  planes viewed along the  $\langle 1\ 1\ 0 \rangle$  zone  
 149 direction of  $\alpha$ -Al which have different tilt angle ( $0\sim 10^\circ$ ) with  $\{1\ 1\ 1\}_{\alpha\text{-Al}}$ . The lattice misfits  
 150 between these  $\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}$  planes of  $\alpha$ -Al and the fixed nucleation substrate ( $(2\ -2\ 2)_{\text{MgAl}_2\text{O}_4}$ ) were  
 151 calculated. The results were shown in Table 1. The lattice parameters of  $\alpha$ -Al and  $\text{MgAl}_2\text{O}_4$   
 152 used are calculated at  $660^\circ\text{C}$  taking into account the thermal expansion of both structures [31-  
 153 32]. With the increased  $\theta$ , the  $d\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}_{\alpha\text{-Al}}$  increases. The very small changes in  $\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}_{\alpha\text{-Al}}$   
 154 indicates the large atomic distances at the interface. If the  $d\left\{\frac{1}{x}\ \frac{1}{x}\ 1\right\}_{\alpha\text{-Al}}$  is analysed using the  
 155 coincidence site lattice (CSL) for the mismatch between the solid  $\alpha$ -Al and the substrates  $\{1\ 1\ 1\}$   
 156 of  $\text{MgAl}_2\text{O}_4$ , then the match due to CSL increases with the increased  $\theta$  ( $0\sim 10^\circ$ ). When the  
 157 tilt angle is  $8.5^\circ$ , same angle as the experimental results, the OR is  $(7\ -7\ 5)_{\alpha\text{-Al}}//\{1\ 1\ 1\}_{\text{MgAl}_2\text{O}_4}$ .  
 158 Therefore, the actual heterogeneous nucleation interface was calculated to be  $(7\ -7\ 5)_{\alpha\text{-Al}}$  and  
 159 modified  $(2\ -2\ 2)_{\text{MgAl}_2\text{O}_4}$  rather than that of  $(1\ -1\ 1)_{\alpha\text{-Al}}//\{1\ 1\ 1\}_{\text{MgAl}_2\text{O}_4}$ . However, it shows that  
 160 the misfit between the  $(7\ -7\ 5)_{\alpha\text{-Al}}$  and the  $(2\ -2\ 2)_{\text{MgAl}_2\text{O}_4}$  is 5.53% which is much bigger than

161 that the misfit (1.36%) between  $(1 -1 1)_{\alpha\text{-Al}}$  and  $(2 -2 2)_{\text{MgAl}_2\text{O}_4}$ . The heterogeneous nucleation  
162 occur at an interface with a larger misfit rather than that with a smaller misfit, indicating some  
163 surface modification on  $\text{MgAl}_2\text{O}_4$ . Therefore, the lattice mismatch between the  $\left\{\frac{1}{x} \frac{1}{x} 1\right\}_{\alpha\text{-Al}}$  and  
164 modified  $(2 -2 2)_{\text{MgAl}_2\text{O}_4}$  need to be reconsidered. The calculation in Table 1 is not suitable for  
165 the modified surface. Other factors that affect the interface structure such as surface roughness,  
166 interfacial segregation need to be considered.

167 The grain refinement shown in Fig.3 indicated that these native  $\text{MgAl}_2\text{O}_4$  particles were potent  
168 to refine the  $\alpha\text{-Al}$  grains after intensive melt shearing. This indicates that the native  $\text{MgAl}_2\text{O}_4$   
169 particles with modified surface are potent for the nucleation of  $\alpha\text{-Al}$ , i.e. the mismatch between  
170 the  $(7 -7 5)_{\alpha\text{-Al}}$  and modified  $(2 -2 2)_{\text{MgAl}_2\text{O}_4}$  did not affect the potency of the particles  
171 significantly. The comparison of interfacial atomic match between the  $(1 -1 1)_{\alpha\text{-Al}}$  on the  $(2 -2$   
172  $2)_{\text{MgAl}_2\text{O}_4}$  with and without the tilt angle was simulated with Crystal Maker software, Figs.4a-  
173 b, and using schematics illustrate the interface atomic matching with the crystal lattice  
174 parameters. The  $\text{MgAl}_2\text{O}_4$  particles were reported to have multiple of possibilities on surface  
175 planes and surface atomic arrangements [33-34]. In this simulation, the surface atoms on the  
176  $(2 -2 2)$  surface planes of  $\text{MgAl}_2\text{O}_4$  particles which formed in Al melts were set to be Al. Fig.4  
177 a shows that the clean  $\{1 1 1\}_{\text{MgAl}_2\text{O}_4}$  has perfect matching with the  $\{1 1 1\}_{\alpha\text{-Al}}$ . However, the  
178 surface of the  $\text{MgAl}_2\text{O}_4$  particles in Al-5Mg-2Si-0.7Mn-1.1Fe was modified by a  $8.5^\circ$  tilt angle  
179 as observed during the heterogeneous nucleation of  $\alpha\text{-Al}$  (Fig.2). Fig.4b shows that when the  
180 interface between  $\alpha\text{-Al}$  was tilted, the parallel plane of  $\alpha\text{-Al}$  with the  $(2 -2 2)$  plane of  $\text{MgAl}_2\text{O}_4$   
181 changes from close-packed  $(1 -1 1)$  to  $(7 -7 5)$  which lower atomic density.

182 As discussed above, the most likely reason for the interfacial modification of  $\{1 1 1\}_{\text{MgAl}_2\text{O}_4}$   
183 is the interfacial segregation. The interfacial segregation changes atomic arrangement above  
184 the  $\text{MgAl}_2\text{O}_4$  particles in the melt by allowing Fe, Si or Mn or other impurity elements to  
185 segregate on the surface or chemically interact with the surface atoms of  $\text{MgAl}_2\text{O}_4$ . The atomic  
186 radii among the possible segregation elements such as Fe, Mn, Si and Al are different, and  
187 some vacancies might be generated which can cause the faceted  $\{1 1 1\}_{\text{MgAl}_2\text{O}_4}$  become rougher.  
188 The interfacial segregation and subsequent roughening on the nucleation substrates changes  
189 the atomic templating. As discussed before, the tilt angle corresponds to a higher indexed  
190 planes of the substrates, which means larger CSL and a rough surface on the modified  
191  $\text{MgAl}_2\text{O}_4$ . Due to limited understanding of heterogeneous nucleation on the rough surfaces, our  
192 initial hypothesis was schematically presented in Fig.4c-d to describe this heterogeneous  
193 nucleation process.

194 Fig.4d shows the case that different elements segregate on the surface of native  $\text{MgAl}_2\text{O}_4$   
195 particles. The number, type and positions of the adsorbed atoms depending on the melt  
196 composition can be different, and Fig.4d only shows one of the possibilities. The atomic  
197 arrangement at the interface is predicted to affect the nucleation, which needs further  
198 investigation. In this case, the higher indexed planes  $((7 -7 5)_{\alpha\text{-Al}})$  as the first templating layer  
199 to accommodate the roughness of the surface due to segregation generated larger coincidence  
200 site lattice (CSL). After a few atomic layer templating, the nucleated solid grows into the crystal  
201 to minimise the interfacial energy.

202 Grain refinement not only requires potent nucleation substrates, but also requires suitable  
203 particle size and size distribution. More importantly, it requires an adequate number density  
204 ( $N_0$ ). In this study, the number density was calculated in non-sheared and sheared cases with  
205 the assumption that each grain has a  $MgAl_2O_4$  as a nucleus (Table 2). According to the grain  
206 size, the number of effective nucleated particles  $N_v$  can be calculated according to the equation:

$$207 \quad N_v = \frac{0.5}{d^3} \quad [35].$$

208 The nucleation efficiency was assumed to be 0.5% in both non-sheared and sheared cases.  
209 Therefore, the particles number densities in these two cases were calculated as  $1.3 \times 10^{12} m^{-3}$   
210 and  $3.0 \times 10^{13} m^{-3}$ , respectively. As reported [36], the number density of  $TiB_2$  particles in  
211 1000 ppm Al-5Ti-1B grain refiner addition is  $7.3 \times 10^{12} m^{-3}$ . The number density of native  
212 oxide particles therefore is adequate to cause grain refinement in Al-alloys.  
213

## 214 5. Conclusions

215 The main results are summarized as:

216 (1) The major naturally formed oxides in Al-5Mg-2Si-0.7Mn-1.1Fe alloy were identified as  
217  $MgAl_2O_4$ . These  $MgAl_2O_4$  particles were {1 1 1} faceted, and have size range from 0.5 to 1  $\mu m$ .

218 (2) A well-defined orientation relationship between  $\alpha$ -Al and  $MgAl_2O_4$  was observed and  
219 identified to be:  $8.5^\circ (-1 \ 1 \ -1)_{\alpha-Al} // (2 \ -2 \ 2)_{MgAl_2O_4}$ , and  $[-1 \ 1 \ 0]_{\alpha-Al} // [-1 \ 1 \ 0]_{MgAl_2O_4}$ .

220 (3) The number density of native  $MgAl_2O_4$  particles is sufficient to enhance the heterogeneous  
221 nucleation of  $\alpha$ -Al in Al-alloys and lead to grain refinement.

222

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226

## 227 References

228 [1] R. Schweinfest, S. Kostlmeier, F. Ernst, C. Elsaser, T. Wagner, M. W. Finnis, Atomistic and  
229 electronic structure of Al/ $MgAl_2O_4$  and Ag/ $MgAl_2O_4$  interfaces, Philos. Mag. A 81 (2001)  
230 927-955.

231 [2] A. Cibula, The effect of C and B in the grain refinement of sand casting in aluminum alloys,  
232 J. Inst. Met. 80 (1951)1-16.

233 [3] B.S. Murty, S.A. Kori, M. Chakraborty, Grain refinement of aluminium and its alloys by  
234 heterogeneous nucleation and alloying, Int. Mater. Rev. 47 (2002) 3-29.

235 [4] T.E. Quested, Understanding mechanisms of grain refinement of aluminium alloys by  
236 inoculation, Mater. Sci. Tech. 20 (2004) 1357-1369.

- 237 [5] M.A. Easton, H. Wang, J.F. Grandfield, D.H. StJohn, E. Sweet, An analysis of the effect of  
238 grain refinement on the hot tearing of aluminium alloys, *Mater. Forum* 28 (2004) 224–229.
- 239 [6] P. S. Mohanty, J. E. Gruzleskit. Mechanism of grain refinement in Aluminium, *Acta Metall.*  
240 *Mater.* 43(5) (1995) 2001-2012.
- 241 [7] F.A. Crossley, L.F. Mondolfo, Mechanism of grain refinement in aluminum alloys, *AIME*  
242 *Trans.* 191 (1951) 1143-1148.
- 243 [8] Z. Fan, Y. Wang, Y. Zhang, T. Qin, X.R. Zhou, G.E. Thompson, T. Pennycook, T.  
244 Hashimoto, Grain refining mechanism in the Al/Al–Ti–B system, *Acta Mater.* 84 (2015)  
245 292-304.
- 246 [9] J.A. Spittle, S. Sadli, The influence of zirconium and chromium on the grain-refining  
247 efficiency of Al—Ti—B inoculants, *Cast Metal.* 7 (1995) 247-253.
- 248 [10] S.A. Kori, B.S. Murty, M. Chakraborty. Influence of silicon and magnesium on grain  
249 refinement in aluminium alloys, *Mater. Sci. Technol.* 15 (1999) 986-992.
- 250 [11] Y. Wang, C.M. Fang, L. Zhou, T. Hashimoto, X. Zhou, Q.M. Ramasse, Z. Fan,  
251 Mechanism for Zr poisoning of Al-Ti-B based grain refiners, *Acta Mater.* 164 (2019) 428-  
252 439.
- 253 [12] Q. Chen, The effect of transition metal additions on double oxide film defects in Al alloy  
254 castings. PhD thesis, University of Birmingham (2016).
- 255 [13] S. Impey, D.J. Stephenson, J.R. Nicholls, A Study of the Effect of Magnesium Additions  
256 on The Oxide Growth Morphologies on Liquid Aluminium Alloys, in *Int. Conf. on the*  
257 *microscopy of oxidation.* University of Cambridge (1990) 238-244.
- 258 [14] K.L. More, P.F. Tortorelli, L.R. Walker, J. Hryn, G. Krumdick, Microstructural evaluation  
259 of dross formation on Mg- and non-Mg- containing Al alloys from industrial furnaces,  
260 *Materials at high Temperature,* 20(3) (2003) 453-460.
- 261 [15] G. Wu, K. Dash, M.L. Galano, K.A.Q. O’Reilly, Oxidation studies of Al alloys: Part II  
262 Al-Mg alloy, *Corrosion Science,* 155 (2019) 97-108.
- 263 [16] H.-T. Li, Y. Wang, Z. Fan, Mechanisms of enhanced heterogeneous nucleation during  
264 solidification in binary Al–Mg alloys, *Acta Mater.* 60 (2012) 1528-1537.
- 265 [17] R. Gopalan, N. K Prabhu, Oxide bifilms in aluminium alloy castings—a review, *Mater. Sci.*  
266 *Technol.* 27 (12) (2011) 1757-1769.
- 267 [18] J. Campbell, Discussion of “Effect of Strontium and Phosphorus on Eutectic Al-Si  
268 Nucleation and Formation of  $\beta$ -Al<sub>5</sub>FeSi in Hypoeutectic Al-Si Foundry Alloys”, *Metall.*  
269 *Mater. Trans. A* 40A (2009) 1009–1010.
- 270 [19] Z. Fan, Y. Wang, Z.F. Zhang, etc. Shear enhanced heterogeneous nucleation in some Mg-  
271 and Al-alloys, *Int. J. Cast Metal. Res.* 22 (1-4) (2009) 318-322.
- 272 [20] Z. Fan, Y. Wang, M. Xia, S. Arumuganathar, Enhanced heterogeneous nucleation in  
273 AZ91D alloy by intensive melt shearing, *Acta Mater.* 57(16) (2009) 4891-4901.
- 274 [21] Z.P. Que, Y.P. Zhou, Y. Wang, Z. Fan, Composition templating for heterogeneous  
275 nucleation of intermetallic compounds, *Solidification Processing* (2017) 158-161.
- 276 [22] Z. Fan, B. Jiang, Y. Zuo, US2013/0228045.

277 [23] Aluminium Association: Standard Test Procedure for Aluminium Alloy Grain Refiners:  
 278 TP-1, Washington DC. 1987.

279 [24] Y. Zuo, B. Jiang, P. Enright, G.M. Scamans, Z. Fan, Degassing of LM24 Al alloy by  
 280 intensive melt shearing, *Int. J. Cast Metal. Res.* 24(5) (2011) 307-313.

281 [25] I. Haginoya, T. Fukusako, Oxidation of Molten Al-Mg Alloys, *Trans. Jpn. Inst. Met.*  
 282 24(9)(1983) 613-619.

283 [26] C.J. Simensen and C. Berg, A survey of inclusions in aluminum, *Alum. Dusseldorf*  
 284 56(1980) 335-40.

285 [27] F. Wang, Z. Fan, Characterization of AlN Inclusion Particles Formed in Commercial  
 286 Purity Aluminum, *Metall. Mater. Trans. A* 50A(2019) 2519-2526.

287 [28] R. Raiszadeh, W.D. Griffiths, A method to study the history of a double oxide film defect  
 288 in liquid aluminum alloys, *Metall. Mater. Trans. B* 37B (2006) 865-871.

289 [29] X. Cao, J. Campbell, The nucleation of Fe-rich phases on oxide films in Al-11.5 Si-0.4  
 290 Mg cast alloys, *Metall. Mater. Trans. A* 34(7) (2003) 1409-1420.

291 [30] Z.P. Que, Y. Wang, Z. Fan, Formation of the Fe-containing intermetallic compounds  
 292 during solidification of Al-5Mg-2Si-0.7 Mn-1.1 Fe alloy, *Metall. Mater. Trans. A* 49 (2018)  
 293 2173-2181.

294 [31] J.W. Arblaster. *Selected Values of the Crystallographic Properties of Elements*, ASM  
 295 International, 2018: 129.

296 [32] [www.msesupplies.com](http://www.msesupplies.com).

297 [33] C.M. Fang, S.C. Parker, G. With, Atomistic simulation of the surface energy of spinel  
 298 MgAl<sub>2</sub>O<sub>4</sub>. *Journal of the American Ceramic Society*, 83(8) (2000) 2082-2084.

299 [34] N.J. Van der Laag, C.M. Fang, G.de With, Geometry of {001} surface of spinel  
 300 (MgAl<sub>2</sub>O<sub>4</sub>): first-principles simulations and experimental measurements, *J. Am. Ceram.*  
 301 *Soc.* 88(6) (2005) 1544-1548.

302 [35] A.L. Greer, A.M. Bunn, A. Tronche, P. V. Evans, D. J. Bristow, Modelling of inoculation  
 303 of metallic melts: application to grain refinement of aluminium by Al-Ti-B, *Acta Mater.* 48  
 304 (2000): 2823-2835.

305 [36] T.E. Quested, A.L. Greer, The effect of the size distribution of inoculant particles on as-  
 306 cast grain size in aluminium alloys, *Acta Mater.* 52 (2004) 3859-3868.

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