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A METHOD FOR SOLVING MOVING  
BOUNDARY PROBLEMS IN HEAT FLOW  
PART II: USING CUBIC POLYNOMIALS.

by

John Crank and Radhey S. Gupta.

## ABSTRACT

A moving grid system has been used to get the solution of the moving boundary problem discussed earlier in Part I, but basing the necessary interpolations on ordinary cubic polynomials rather than splines. The computations are much more economical and the results obtained are also found to be more satisfactory.

A Method for Solving Moving Boundary Problems  
in Heat Flow : Part II Using Cubic Polynomials.

John Crank and Radhey S. Gupta  
Department of Mathematics, Brunel University, Uxbridge.

1. Introduction.

The present authors [1 ] discussed a moving boundary problem arising from the diffusion of oxygen in an absorbing medium and made use of finite difference formulae for unequal intervals in the region of the moving boundary together with a Taylor's series expansion. An early finite difference method [2] proposed the use of the variable time step chosen so that the boundary always moves from one line of the space grid to the neighbouring one in a single time step. Another method [3] maintained a fixed number of equal space intervals between the surface of the medium and the moving boundary, the size of the interval being correspondingly adjusted. The present authors [4] suggested the use of a moving grid system which moves with the velocity of the moving boundary. The method made use of cubic splines to interpolate between the grid points.

In the present paper same idea of a moving grid system is employed to solve the problem discussed in [1 ] or [4] but the necessary interpolations are performed by using ordinary cubic polynomials rather than splines. This avoids solving the tridiagonal set of equations in Part I and the results thus obtained also show a superiority over the results obtained in [4].

For the sake of completeness of the paper we repeat sections 2 and 3 of [4].

## 2. An Example,

We shall introduce the new method by referring to a practical problem which the authors described in detail in the earlier paper [1]. Expressed in non-dimensional terms we require the solution of the equation

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} - 1, \quad 0 \leq x \leq \delta, \quad t \geq 0. \quad (1)$$

with the boundary conditions

$$\frac{\partial u}{\partial x} = 0, \quad x=0, \quad t \geq 0, \quad (2)$$

$$u = \frac{\partial u}{\partial x} = 0, \quad x = \delta(t), \quad t \geq 0, \quad (3)$$

and the initial condition

$$u = \frac{1}{2}(1-x), \quad 0 < x < 1, \quad t = 0, \quad (4)$$

where  $\delta(t)$  denotes the position of the moving boundary at time  $t$ .

## 3. A Moving Grid System.

Traditionally, we divide the region  $0 \leq x \leq 1$  into  $n$  intervals each of width  $\Delta x$  such that  $x_{i+1} = i\Delta x$ ,  $i = 0, 1, \dots, n$  and  $n\Delta x = 1$ . By some numerical procedure we advance the solution in finite time steps  $\Delta t$ , starting from the known solution at  $t = 0$ , given by (4).

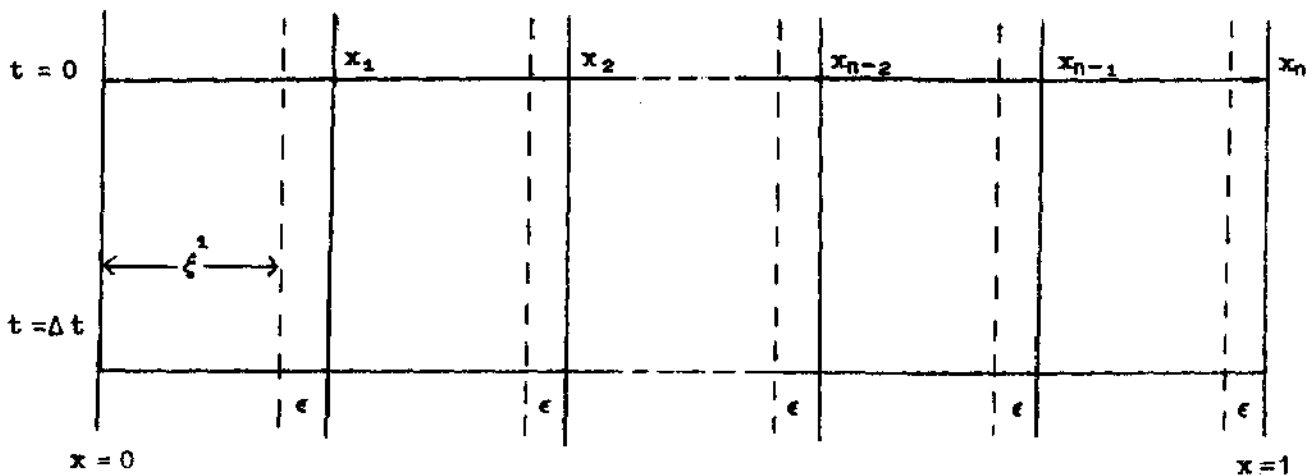


Fig.1 Moving Grid

We denote by  $U_i^j$  the values of  $u$  at  $(i\Delta x, j\Delta t)$ ,  $j=0, 1, 2, \dots$ , so that in the first interval  $\Delta t$  we evaluate  $U_{n-1}$  and also the new position of the boundary which has moved from  $x=1$  to  $x=1-\varepsilon$ , say, as in Figure 1. We now move the whole grid a distance  $\varepsilon$  to the left as indicated by the broken lines, and we wish to evaluate values of  $U^0$  and the second space derivatives at each of the points  $x_1 - \varepsilon, x_2 - \varepsilon, \dots, x_{n-1} - \varepsilon, 1 - \varepsilon$ . We describe another method for doing this, using ordinary cubic polynomials for interpolation between the points  $x_0, x_1, x_2, \dots, x_{n-1}, 1$  at  $t=0$ . We can then proceed in similar fashion to  $2\Delta t$  and in general to  $j\Delta t$  ( $j=3, 4, \dots$ ) provided we include a modification to allow for the unequal interval  $\xi^j$  at the  $j$ th time step near the surface  $x=0$ .

#### 4. Forward Difference Polynomial (F.D.P.) Method.

In this method we retain the same idea of a moving grid system but avoid solving the tridiagonal set of equations of FDS method [4]. Instead, the second space derivatives are calculated from the values of  $u$  by using the simple 3-point finite-difference formulae. Interpolation between any two grid points is then based on a cubic polynomial which satisfies the function values and the second derivatives at the two grid points.

Thus, we represent  $u(x)$  between the two points  $x_i, x_{i+1}$  by

$$u_{i,i+1} = \alpha + \beta x + \gamma x^2 + \mu x^3, \quad (5)$$

where  $\alpha = \alpha(i, i+1)$  etc.

We employ the usual expressions

$$U''_i = \frac{U_{i-1} - 2U_i + U_{i+1}}{(\Delta x)^2}, i = 1, 2, \dots, n, \tag{6}$$

and at the surface  $x = 0$ ,

$$U''_0 = \frac{2}{\xi^2} (U_0 - U_1), \tag{7}$$

where  $\xi = x_1 - x_0$ .

At  $x = x_1$  we use a formula of the same type but generalised to allow for the unequal interval  $\xi$ , namely

$$U''_i = 2 \left\{ \frac{U_0}{\xi(\xi + \Delta x)} - \frac{U_1}{\xi \Delta x} + \frac{U_2}{\Delta x(\xi + \Delta x)} \right\}. \tag{8}$$

From (5.1) we obtain

$$U_{i,1+\ell} = 6\mu x + 2y, \tag{9}$$

and thus by inserting values  $U_i, U_{i+1}, U_i, U_{i+1}$  into (5) and (9) we derive the coefficients  $\alpha, \beta, \gamma, \mu$  and hence determine the polynomial for the interval  $x_i$  to  $x_{i+1}$

For the interval near the moving boundary we make use of the conditions derived in [1] which are given by

$$\frac{\partial^2 u}{\partial x^2} = 1, \frac{\partial^3 u}{\partial x^3} = -\frac{\partial \delta}{\partial t}, \frac{\partial^4 u}{\partial x^4} = \left(\frac{\partial \delta}{\partial t}\right)^2 \dots \text{etc.}, \tag{10}$$

at the moving boundary giving  $U''(x_n) = 1$ .

Assuming the function values to be known at any time  $j \Delta t$  when the distance of the moving boundary from the surface  $x = 0$  is  $\xi^j + r \Delta x$  the method proceeds as follows.

Obtain the second derivatives  $U''(x_i), i = 0, 1, \dots, (r + 1)$  from (6),(7),(8) and (10). The value of  $U_r^{j+1}$  i.e. at

the point neighbouring the moving boundary, follows from the simple explicit relationship

$$\frac{U_r^{j+1} - U_r^j}{\Delta t} = U(\chi_r^j) - 1, \quad (11)$$

where  $U^*(\chi_r^j)$  denotes the value of the second derivative at  $x_r$  at  $t = j\Delta t$ .

The Taylor's series for  $U_r$  obtained by expanding about the moving point can be written as in [4],

$$U_r = U(\delta) - \ell \left( \frac{\partial u}{\partial x^2} \right)_{x=\delta} + \frac{1}{2} \ell^2 \left( \frac{\partial^2 u}{\partial x^2} \right)_{x=\delta} - \frac{1}{6} \ell^3 \left( \frac{\partial^3 u}{\partial x^3} \right)_{x=\delta} + \dots,$$

where  $\ell (0 \leq \ell \leq \Delta x)$  is the distance of the moving point from  $U_r$ .

Using (3) and (10) and assuming that the boundary is not moving too quickly, the above relation gives to a reasonable accuracy

$$\ell = \sqrt{2U_r}. \quad (12)$$

Therefore, once  $U_r^{j+1}$  is known from (11), we can find the position of the moving boundary from (12). Hence, the movement,  $\varepsilon^{j+1}$ , of the boundary in time  $\Delta t$ , from  $j\Delta t$  to  $(j+1)\Delta t$  is given by

$$\varepsilon^{j+1} = \Delta x - \ell^{j+1}. \quad (13)$$

Having got  $\varepsilon$  from (13) we then interpolate the values of  $u(x)$  at  $t = j\Delta t$  at the points  $x_1 - \varepsilon, x_2 - \varepsilon, \dots, x_r - \varepsilon, \delta - \varepsilon$

using (5) and the corresponding second derivatives from the linear relationship

$$\frac{U^*(x_{i+1}^j) - U^*(x_i^j)}{x_{i+1}^j - x_i^j} = \frac{U^*(x_{i+1}^j) - U^*(x_i^j)}{x_{i+1}^j - x_i^j} \quad (14)$$

where  $x_i^j$  denotes the  $i$ th mesh point such that  $x_i^j = \xi^j + (i-1)\Delta x$  at time  $j\Delta t$ ;  $x_i^j \leq x \leq x_{i+1}^j$  and  $i = 0, 1, \dots, r$ .

The values of  $u(x)$  at  $x_1, x_2, \dots, x_r$ , at time  $(j+1)\Delta t$  follow at once from

$$\frac{U^{j+i}(x_i^{j+i}) - U^j(x_i^j - \epsilon^{j+i})}{\Delta t} = U^*(x_i^j - \epsilon^{j+i}) - 1, \quad (15)$$

$$x_i^{j+i} = x_i^j - \epsilon^{j+i}, \quad i = 1, 2, \dots, r,$$

together with

$$\frac{U_0^{j+1} - U_0^j}{\Delta t} = U^*(x_0^j) - 1, \quad \text{at the surface } x = 0. \quad (16)$$

We should remember that the space interval  $x_1 - X_0 = \xi$  is not fixed and varies from one time step to the next.

We proceed in steps  $\Delta t$  in this way testing  $\xi$  at each

step for stability. When  $\frac{\Delta t}{\xi^2} \geq \frac{1}{2}$  we replace  $\xi$  by  $\Delta x + \xi$  to get values at the next time step and proceed as before. A stability analysis for this method has been appended at the end of the paper.



5. Results and Discussion.

Let us rewrite the expression for the analytical solution obtained in [1] for small times when the boundary  $x = 1$  has not moved to the working accuracy

$$U(x, t) \sim \frac{1}{2}(1-x)^2 - 2\sqrt{\frac{t}{w}} \exp \left\{ -\left( -\frac{x}{2\sqrt{t}} \right)^2 \right\} + \text{xerfc} \left( \frac{x}{2\sqrt{t}} \right), \quad (17)$$

$$0 \leq x \leq 1.$$

We start the FDP and the FGL\* solutions from the values taken from (17) at  $t = 0.025$  and give a comparison for the positions of the moving boundary and the surface concentrations in Tables I and II respectively. The figures throughout for corresponding step size show a very good agreement in both cases. The corresponding values obtained by using cubic splines in Part I are also presented for comparison in Tables I and II.

Apart from getting superior results by the FDP method the effort involved in using it, is appreciably less than for the FDS method essentially because the latter involves the solution of a tridiagonal set of equations at each time step.

Considering the important problem of roughness in the positions of the moving boundary which is produced by the FGL method near the times where the process used to calculate the concentration in the neighbourhood of the moving point is transferred one space interval towards the surface  $x = 0$ . We give in Table III

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\* Fixed Grid Lagrange, the numerical method used in [1] •

the positions of the boundary at and around such times of shifting the interval in the FGL method along with the corresponding figures from the FDP method. The irregularities produced in the former method are clearly visible while their counterparts show a smooth behavior throughout.

Table IV gives a comparison of the surface concentrations obtained by the FDP and the FGL methods at and around times when the first space interval  $\xi$  in the former is increased to  $\xi + \Delta x$  for the succeeding computations. It is interesting to note that the differences in the concentrations show no sign of irregularities.

TABLE I

Comparison of  $10^4\delta$  at different times. All solutions start from the analytical solution at  $t = 0.025$ .

Method \ Time	0.040	0.060	0.100	0.120	0.140	0.160	0.180	0.185
FGL $\Delta x=0.05$	9992	9918	9346	8781	7966	6799	4942	4178
$\Delta x = 0.10$	9988	9904	9308	8734	7912	6725	4830	4114
FDP $\Delta x = 0.05$	9992	9918	9344	8780	7968	6798	4948	4258
FDS $\Delta x= 0.10$	9993	9920	9327	8739	7892	6664	4680	3917

TABLE II

Comparison of  $10^4U$  at the surface  $x=0$ , at different times. All solutions start from the analytical solution at  $t = 0.025$ .

Method \ Time	0.040	0.060	1 0.100	0.120	0.140	0.160	0.180	0.185
FGL $\Delta x = 0.05$	2742	2234	1430	1089	777	486	216	151
$\Delta x = 0.10$	2745	2238	1434	1093	780	490	219	155
FDP $\Delta x = 0.05$	2742	2234	1429	1089	776	486	216	151
FDS $\Delta x= 0.10$	2736	2277	1424	1083	771	481	210	145

TABLE III

Table showing the irregularities in the position of the moving boundary, calculated by the FGL method. Comparatively smooth figures are shown for the FDP method ( $\Delta x = 0.10$ ),

Time	FG-L Method			FDP Method		
	$10^4\delta$	$-\Delta$	$-\Delta^2$	$10^4\delta$	$-\Delta$	$-\Delta^2$
0.110	9099	29		9104		
	9070	30	1	9076	28	0
	<u>9040</u>	30	0	<u>9048</u>	28	1
	9010	26	-4	<u>9019</u>	29	0
	8984			8990	29	
0.137	8141	52		8145		
	8089	55	3	8100	45	1
	<u>8034</u>	40	15	<u>8054</u>	46	0
	7994		0	8008	46	2
	7954			7960		
0.154	7277			7256	61	
	7204	73		7195		
	<u>7124</u>	80	7	<u>7132</u>	63	2
	7037	87	-35	7068	64	1
	6985	52		7002	66	2
0.167	6396			6343	82	
	6306	90	13	6261		
	<u>6203</u>	103	55	<u>6177</u>	84	2
	6045	158	-92	6090	87	1
	5979	66		6002	88	
0.176	5499			5520		
	5393	106	19	5415	105	4
	<u>5268</u>	125	123	<u>5306</u>	109	4
	5020	248	-165	5193	113	
	4937	83		5077	116	3
0.184	4652	114		4563		
	4538	132	18	4421	142	
	<u>4406</u>	392	260	<u>4271</u>	150	8
	4014	102	-290	<u>4114</u>	157	7
	3912			3948	166	9

NOTE : The data are tabulated at an interval of time  $\Delta t = 0.001$ . The underlined values correspond to the times when the interpolation process near the moving boundary is transferred one step to the left.

TABLE IV

Table showing the smoothness of the surface concentrations calculated by the FDP method at times when the first interval is increased by  $\Delta x$ . Corresponding figures for the FGL method are given for comparison ( $\Delta x = 0.10$ ).

Time	FDP Method		FGL Method	
	$10^4 U_0$	$-\Delta$	$10^4 U_0$	$-\Delta$
0.093	1599		1598	
	1580	19	1580	18
	1562	18	1561	19
	1543	17	1543	18
	1525	18	1524	19
0.127	1013		1013	
	997	16	997	16
	321	16	981	16
	965	16	965	16
	950	15	950	15
0.148	691		691	
	676	15	677	14
	<u>662</u>	14	<u>662</u>	15
	647	15	647	15
	633	14	633	14
0.163	476		476	
	462	14	462	14
	448	14	448	14
	434	14	435	13
	420	14	421	14
0.174	325		326	
	312	13	312	14
	298	14	299	13
	285	13	286	13
	272	13	272	14
0.182	219		220	
	206	13	207	13
	<u>193</u>	13	<u>194</u>	13
	180	13	181	13
	168	12	168	13

NOTE: The data are tabulated at an interval of time  $\Delta t = 0.001$ . The underlined values correspond to the times when the first space interval is increased by  $\Delta x$ .

## 6, Generalisation.

We consider the same latent heat type problem as discussed in [4]. In non-dimensional form the relevant equations are ,

$$\frac{\partial u}{\partial t} = \frac{\partial^2 u}{\partial x^2} , \quad 0 \leq x \leq \delta(t) \quad ; \quad (18)$$

$$\frac{\partial u}{\partial x} = -1 , \quad x = 0 , \quad t \geq 0 \quad ; \quad (19)$$

$$u = 0, \quad x = \delta(t), \quad t \geq 0 \quad ; \quad (20)$$

$$\frac{\partial u}{\partial x} = - \frac{\partial \delta}{\partial t} = - \delta'' , \quad x = \delta(t) ; \quad (21)$$

$$\delta=0, \quad t = 0. \quad (22)$$

Let us assume that the values of  $U_0, U_1, \dots, U_r, U_{r+1}$  are known at the  $j$ th time level and the position of the moving boundary is also known at that time which is given by  $\delta^j = \zeta^j + r \Delta x$ . The width of all the meshes is  $\Delta x$  except the first one which is  $\zeta^j$ .

The second derivatives at the surface and the first mesh points, at the  $j$ th time level, can be computed by (7) and (8) respectively while at the intermediate points they can be obtained by (6).

To get second derivative at the last mesh point i.e. the moving boundary we differentiate (20) with respect to  $t$  and use (18) and (21) such that

$$\left( \frac{\partial^2 u}{\partial x^2} \right)_{x = \delta} = \left( \frac{\partial \delta}{\partial t} \right)^2 = \frac{1}{\delta} , \quad (23)$$

giving  $U''(x_{r+1}) = \dot{\delta}^2$  where  $\delta$  is a function of  $t$ .

But the Taylor's expansion for  $U_r$  about the moving boundary, after making the appropriate substitutions, gives as in [4] ,

$$\dot{\delta} = -1 + \sqrt{1 + 2U_r}, \quad (24)$$

which in turn, using (23) gives

$$U''(x_{r+1}) = \{-1 + \sqrt{1 + 2U_r}\}^2. \quad (25)$$

The new position of the moving boundary at the  $(j+1)^{\text{th}}$  time level is determined from (24) after replacing  $\delta$  by a forward finite difference i.e.

$$\frac{\delta^{j+1} - \delta^j}{\Delta t} = 1 + \sqrt{1 + 2U_r^j}. \quad (26)$$

The interpolations for the value of  $u$  and its second derivative for  $x_i \leq x \leq x_{i+1}$  ,  $i = 0, 1, \dots (r-1)$  can be performed by using (5) and (14.) respectively.. But for the interval next to the moving boundary the relations (20) and (25) are to be used for the desired interpolations.

It should again be remembered that as the boundary  $\delta(t)$  is moving forward the first interval  $\xi$  becomes larger and larger with time. As soon as it becomes greater than  $\Delta x$  we should break it into two intervals making the second to be of width  $\Delta x$  and the interval

nearest to the surface  $x = 0$  to be of width  $\xi - \Delta x$ .

The value of  $u$ , at the new mesh point, has to be interpolated using (5).

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## APPENDIX

Stability Analysis for F.P.P.Method.

Following the same argument as in the previous paper [1], it is easy to show that for stability, we require the largest modulus of the eigenvalues of the square matrix A to be less than unity where A is given by

$$\underline{A} = \begin{bmatrix} \left(1 - \frac{2\Delta t}{\xi^2}\right) & \frac{2\Delta t}{\xi^2} & & & \\ \frac{2\Delta t}{\xi(\xi + \Delta x)} & \left(1 - \frac{2\Delta t}{\xi\Delta x}\right) & \frac{2\Delta t}{\Delta x(\xi + \Delta x)} & & \\ 0 & r & (1-2r) & r & \\ & & \cdot & \cdot & \cdot \\ & & & & r(1-2r) \end{bmatrix}$$

Applying Brauer's theorem as in [1] to the first and second rows of  $\underline{A}$  we get

$$(i) \quad \left| \lambda - \left(1 - \frac{2\Delta t}{\xi^2}\right) \right| \leq \frac{2\Delta t}{\xi^2} \quad \text{giving} \quad \frac{\Delta t}{\xi^2} \leq \frac{1}{2} \quad \text{and}$$

$$(ii) \quad \lambda - \left( 1 - \frac{2 \Delta t}{\xi \Delta x} \right) \leq \frac{2 \Delta t}{\Delta x \xi} - \frac{\Delta t}{\xi \Delta x} \leq \frac{1}{2},$$

respectively.

When  $\xi < \Delta x$ , the stability condition clearly is  $\frac{\Delta t}{\xi^2} \leq \frac{1}{2}$ . However,

when  $\xi \geq \Delta x$  the conditions (i) and (ii) are automatically satisfied

since we have  $\frac{\Delta t}{\Delta x^2} \leq \frac{1}{2}$  for the explicit scheme at the intermediate

points.